## Appendix K

# Technical Memorandum I-5 JBLM Vicinity Transportation Operations and Safety Summary 

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# I-5 JBLM Vicinity Congestion Relief Study 

Technical Report<br>I-5 JBLM Vicinity Transportation Operations and Safety Summary

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## I-5 JBLM Vicinity Transportation Operations and Safety Summary

### 1.0 Background

Interstate 5 (I-5) is a national highway of strategic importance as it extends from the US/Mexican Border to the US/Canadian border. It is the primary highway for the movement of goods and people traveling north and south on the west coast of the United States. I-5 is one of the most significant freight corridors in Washington State and is essential to the economic vitality of the Puget Sound region. Within the study area, I-5 serves a function in national defense by providing access to Joint Base Lewis-McChord (JBLM) and the State's National Guard at Camp Murray.

Over the past several years, traffic has increased along the entire l-5 corridor. Within the study area in south Pierce County, traffic has also grown. Between 1986 and 2011 the average annual daily traffic (AADT) on I-5 at DuPont increased 72 percent ( 68,600 to over 118,000 vehicles per day.) During this time, JBLM has evolved into a strategic military base, Camp Murray has expanded, and the City of Lakewood was established, and the cities of Lakewood, DuPont and Steilacoom have all grown in both population and employment.

In 2012, the Washington State Legislature appropriated funding to prepare the studies and analyses necessary to identify the causes and potential solutions for chronic congestion on l-5 in the vicinity of JBLM. This work included the I-5 Corridor Feasibility Study, completed in January 2014 and the Multimodal Alternatives Analysis Study, completed in March 2015. These studies identified mainline and interchange capacity scenarios and examined local street and transit options to reduce congestion and improve mobility along l-5.

As part of the Connecting Washington Program, the Washington State Legislature in 2015 approved design, right of way and construction funds for the I-5 JBLM Corridor Improvements. Figure 1 indicates the vicinity map for the project.

### 2.0 Study Area for Traffic Analysis

The Project Corridor study area generally includes I-5 between Mounts Road (Exit 116) on the south and Gravelly Lake Drive (Exit 124) on the north and includes the roads that access, parallel or influence this facility. Within this study area, I-5 is a divided interstate highway with three through lanes in each direction south of Thorne Lane and four through lanes in each direction north of Thorne Lane. All lanes are unmanaged general purpose lanes. There are seven interchanges in this roughly eight-mile study area (Exits 124, 123, 122, 120, 119, 118 and 116).

Figure 1: Project Vicinity Map


Build Alternative (North Study Area)
South Study Area

Figure 1.1-1
Project Vicinity Map

While the Project Corridor study area boundary includes the entire I-5 corridor through the JBLM vicinity, implementation of improvements would occur in phases. The northern portion of the corridor (referred to as he North Study Area), is generally situated between SteilacoomDuPont Road (Exit 119) and Gravelly Lake Drive (Exit 124). A project-specific Build Alternative has been defined in this area. The Build Alternative includes modifications to the freeway mainline and interchanges between the vicinity of the Center Drive interchange (Exit 118) and the Gravelly Lake Drive interchange (Exit 124). They include two primary interchanges that would be reconstructed and four other study area interchanges that would be influenced by the I-5 mainline improvements.

## Primary Interchanges Rebuilt with the Build Alternative

- I-5/Berkeley Street interchange (Exit 122)
- I-5/Thorne Lane interchange (Exit 123)

Interchanges Influenced by the Build Alternative

- Center Drive interchange (Exit 118)
- Steilacoom-DuPont Road interchange (Exit 119)
- Main Gate (41st Division Drive) interchange (Exit 120)
- I-5/Gravelly Lake Drive interchange (Exit 124)

The geographic coverage of the Build Alternative footprint is illustrated in Figure 2. NEPA environmental documentation and a corresponding Interchange Justification Report (IJR) for interstate access modifications have been prepared for this corridor segment. This report supports and provides added information for the Build Alternative analysis.

In the southern portion of the corridor, generally located between Mounts Road (Exit 116) and Steilacoom-DuPont Road (Exit 119), a specific build alternative has not been defined. This portion of the corridor is referred to as the South Study Area and has been evaluated at a corridor level. When a specific build alternative is defined more detailed analysis of traffic operations and safety will be conducted in the South Study Area.

Within the study area, I-5 is a divided interstate highway with three through lanes in each direction south of Thorne Lane and four through lanes in each direction north of Thorne Lane. These lanes are open to all traffic. Northbound and southbound auxiliary lanes are located between the Center Drive and Steilacoom-DuPont Road interchanges. A southbound auxiliary lane is also located between Center Drive and Mounts Road. In 2014, WSDOT added a southbound auxiliary lane between Thorne Lane and Berkeley Street as part of the TIGER III improvement project.

Through the study area, l-5 is physically constrained with secure military installations (JBLM and Camp Murray) on both sides and an active rail line paralleling immediately to the northwest. Alternative routes to move regional traffic are severely limited by the size of JBLM, and further

Figure 2: Proposed Build Alternative

limited by bodies of water, sensitive environmental areas, and locations of sites of archaeology or cultural significance. Because of security restrictions, access through the military installations is limited and alternative travel routes would require long detours.

Between mileposts 117.5 and 125.6 (essentially Center Drive to Gravelly Lake Drive), I-5 is situated on an easement whose ownership is retained by the Department of Defense (DoD). Changes to the existing easement to accommodate freeway improvements will require approval from DoD which can be a lengthy and complicated process.

### 3.0 Analysis of Existing Traffic Conditions

A summary of the existing l-5 traffic operations, including travel demand, travel speeds, congestion and travel times, is presented below. The analyses and procedures that were followed to evaluate existing and future operations used Synchro and Sidra software in accordance with the Highway Capacity Manual (HCM). The traffic analysis assumptions for this project are summarized in the Methods \& Assumptions Document for the I-5 Joint Base Lewis-McChord Vicinity Interchange Justification Report \& Environmental Documentation, contained in Appendix A.

### 3.1 Existing I-5 Traffic Analysis

Based on existing traffic counts collected in 2013, AM and PM peak hour two-way traffic volumes along the I-5 corridor ranged from approximately 7,500 vehicles to 10,900 vehicles. Figure 3 shows the AM and PM peak hour vehicles along I-5 by direction. Using 1,800 vehicles per hour as a maximum practical capacity per lane, the three-lane section has a maximum capacity of 5,400 vehicles and the four-lane section has a capacity of 7,200 vehicles (as indicated by the shaded areas on the charts). It is important to note that because of the slow speeds, stop-and-go traffic, and frequent lane changes, the actual volume that can be accommodated is below the practical capacity of I-5.

During the AM peak hour, the northbound lanes are at or near capacity from Center Drive to Thorne Lane. During the PM peak hour, the southbound lanes are at or near capacity south of the Main Gate Interchange and the northbound lanes are at or near capacity between Berkeley Street and Thorne Lane.

This level of traffic volume along the l-5 corridor together with the reduction in travel lanes at Thorne Lane creates lane turbulence and congestion that:

- Reduces the gap distance between vehicles
- Makes it more difficult for drivers to change lanes safely
- Causes drivers to slow down or even stop as other drivers try to change lanes with smaller gaps
- Results in higher number of rear-end and sideswipe collisions through this area of I-5

Figure 3: 2013 AM and PM Peak Hour Volumes on I-5 from Center Drive to Gravelly Lake Drive



### 3.2 Travel Demand along I-5

Since the last widening of I-5 through the project area in 1975, there have been significant increases in traffic volumes and accompanying congestion along l-5 in the JBLM vicinity. This growth is associated with increased through traffic, local community development and JBLM
commute patterns. As shown in Figure 4 and based on output from the study area Mesoscopic model, over 88 percent of PM peak hour demand could use I-5 in the 2013 analysis base year. This means that approximately 12 percent of the persons who wanted to travel on I-5 during the PM peak hour could not do so because there was insufficient physical space for them to get on the highway. These trips likely spread into the hours adjacent to the PM peak, lengthening the overall multi-hour peak period.

Figure 4: Peak Hour Travel Demand Met on I-5 - Center Drive to Gravelly Lake Drive

## Travel Demand on I-5 Met in 2013 during AM Peak Hour

Travel Demand on l-5 Met in 2013 during PM Peak Hour


- Demand based on person miles of travel estimate from Mesoscopic travel model.


### 3.3 Average I-5 Travel Speeds and Congestion

Average travel speed along the l-5 corridor is a factor that WSDOT uses to illustrate congestion. In WSDOT's Highway System Plan 2007-2026, WSDOT uses 70 percent of posted speed (42 mph ) to signify when congestion occurs at level of service (LOS) $F$ (the shaded areas on Figure 5 are speeds below 70 percent of posted speeds). As can be observed from Figure 6, travel speeds in 2013 along I-5 in the AM peak hour are above 42 mph . However, during the PM peak hour in 2013, there are several segments of I-5 that fall below 42 mph .

Figure 5: 2013 AM and PM Peak Hour Average Travel Speed on I-5
AM Peak Hour Travel Speeds along I-5-2013
Center Drive to Gravelly Lake Drive


PM Peak Hour Travel Speeds along I-5-2013 Center Drive to Gravelly Lake Drive


In the southbound direction average PM speeds are below 42 mph from Gravelly Lake Drive to Steilacoom-DuPont Road with the segment from Thorne Lane to Main Gate being near 20 mph . In the northbound direction, average PM speeds are below 42 mph between SteilacoomDuPont Road and Thorne Lane. These low average speeds signify that several areas along l-5 in the JBLM vicinity have slow moving vehicles with periods of stop-and-go traffic.

Figure 6: Average Travel Speeds on I-5 during the 2013 PM Peak Period


### 3.4 Hours of Congestion along I-5

To estimate how many hours of congestion might occur along l-5, an operational analysis was conducted using INRIX travel data and this project's Mesoscopic Model to estimate travel speeds along l-5 for a six-hour AM peak period and a six-hour PM peak period. Figure 7 illustrates the duration of slow speeds along l-5 at differing locations during the 2013 PM peak period on a typical weekday. The PM peak period that was evaluated ran from 2:00 PM to 8:00 PM. Congestion in both the northbound and southbound directions is shown. As indicated in the figure there are several areas where speeds fell below 42 mph , and for extended periods even below 20 mph . It also shows that these slow speeds extend well past the PM peak hour. In 2013, congestion during the PM peak period lasted for about three hours.

Figure 7: Average Travel Speeds on I-5 during the 2013 PM Peak Period - Nisqually to SR 512


Based on the INRIX and model data, estimates were made of the number of hours the travel speed operated below 70 percent of posted speed or 42 mph . Based on the analysis, less than one hour of congestion occurred during the AM peak period in 2013 (not illustrated). During the PM peak period, several hours of congestion occur along I-5. At experienced by drivers today, this congestion can last from two to 3.5 hours. The hours of congestion during the PM peak period are illustrated in Figure 8.

Figure 8: Hours of Congestion on I-5 during 2013 PM Peak Period - Center Drive to Gravelly Lake Drive

PM Peak Hours of Congestion along I-5-2013 Center Drive to Gravelly Lake Drive


### 3.5 On- and Off-Ramp Volumes along I-5

One of the causes for congestion along l-5 through the JBLM area is the high volume of traffic switching lanes to enter and exit I-5. As shown in Figure 9, it can be observed that for the southbound direction during the AM peak hour, there are over 500 vehicles exiting at Thorne Lane, Berkeley Street, Main Gate and Steilacoom-DuPont Road interchanges. At the same time, there are over 500 drivers entering l-5 from Gravelly Lake Drive, over 300 from Main Gate and over 400 from Steilacoom-DuPont Road. All this traffic cannot be accommodated in the outside lane at the same time, so the exiting drivers must merge right from other lanes before their exit and entering drivers must merge left to clear the outside lane. These heavy merging movements are further complicated for southbound traffic entering north of Thorne Lane, as it must not only merge with the exiting traffic but also must then shift lanes to get past the Thorne Lane Interchange where the outside lane ends, reducing I-5 from four lanes to three lanes.

Figure 9: 2013 AM and PM Peak Hour On- and Off-Ramp Volume on I-5 - Center Drive to Gravelly Lake Drive

2013 AM Peak Hour On and Off-Ramp Volumes along I-5 Center Drive to Gravelly Lake Drive


2013 PM Peak Hour On and Off-Ramp Volumes along I-5 Center Drive to Gravelly Lake Drive


- 2013 SB ■ 2013 NB

Similarly, during the PM peak hour in the northbound direction, there are over 500 vehicles merging onto $\mathrm{I}-5$ at Steilacoom-DuPont Road, Main Gate, and Gravelly Lake Drive and over 1,000 vehicles merging onto l-5 at Berkeley Street and Thorne Lane. At the same time, there are over 500 vehicles exiting l-5 at Steilacoom-DuPont Road and Gravelly Lake Drive. All of this traffic cannot be in the outside lane at the same time, so drivers frequently change lanes as part of entering and exiting l-5.

These heavy lane change movements cause traffic to slow, increase congestion, result in an average of more than one traffic collision per day, and reduce the overall traffic throughput in the JBLM area.

To illustrate the impact of the on and off traffic merging and weaving, two locations are illustrated below. Figure 10 shows northbound weaving between Berkeley Street and Gravelly Lake Drive during a typical 2013 PM peak hour. Within this 1.5-mile distance, nearly 3,500 drivers are engaged in merging on or off the highway and weaving with existing through traffic which almost doubles the 1,800-vehicle capacity of the outside lane.

Figure 11 shows the high levels of weaving and merging that occur during the PM peak hour in the southbound direction between Steilacoom-DuPont Road and Mounts Road. Within this 1.5mile segment of the freeway there are nearly 3,100 drivers, merging and weaving across travel lanes to enter or exit the freeway, well over the 1,800 -vehicle capacity of the outside lane.

### 3.6 Short-Trip Traffic on I-5

Because of the high security military installations, I-5 is the main and essentially only traffic artery through the area for through trips, regional trips and short trips. As a result, there are several locations that have a significant volume of trips that begin and end within the project limits. Many of these short trips are military personnel living off-Base with their families in Lacey, DuPont, Steilacoom, Lakewood or other nearby communities, who generally use the gates closest to where they are stationed on the military base. Many of these short trips use I-5 as there are few to no alternatives for traveling between destinations within the study area.

Other short trips are to and from the Tillicum and Woodbrook neighborhoods. Because of the secure military base around these neighborhoods, these residents use I-5 to reach their destinations in Lakewood and other areas. Overall, these short trips contribute to the congestion and safety problems experienced in the corridor by increasing l-5 traffic volumes and contributing to the high level of weaving and merging activity.

Figure 10: 2013 PM Northbound On- and Off-Ramp Volumes on I-5 - Berkeley Street to Gravelly Lake Drive


Figure 11: 2013 PM Peak Hour Southbound On- and Off-Ramp Volumes on I-5 - Steilacoom-DuPont Road to Mounts Road


### 3.7 Factors affecting Existing Traffic Conditions along I-5

Several factors affect traffic operations along I-5 and contribute to the chronic traffic congestion in the JBLM vicinity. These factors include:

- Existing and growing traffic demand and associated congestion during peak periods of the day along I-5 and at study area interchanges. Between 1986 and 2011, daily traffic volumes on l-5 in the study area increased by 73 percent, from just under 68,000 vehicles to over 118,000 vehicles. This growth is associated with increased through traffic, local community development, and JBLM commute patterns. These higher traffic volumes reduce the gap distances between vehicles, make it more difficult for drivers to change lanes safely and to recover from traffic crashes, and cause drivers to slow down or stop as other drivers try to change lanes with smaller gaps.
- Few alternate routes through the secure military installations, along with environmental and right-of-way constraints, limit opportunities to travel between Thurston County and Tacoma/Seattle.
- Physical limitations and constraints of I-5 through the study area including:
- Change in the number of traffic lanes on l-5 at the Thorne Lane interchange (eight lanes north of Thorne Lane, six lanes south of Thorne Lane).
- Several closely spaced I-5 interchanges (six) over a short distance ( 6.7 miles) between the Center Drive interchange and the Gravelly Lake Drive interchange.
- Physical limitations of the interchanges with narrow bridges that constrain opportunities to increase highway capacity.
- Adjacent rail line that limits highway improvement options.
- Heavy on- and off-ramp volumes at the interchanges between Center Drive and Gravelly Lake Drive. Entering and exiting traffic represents about half of the total traffic along I-5 in the study area. This traffic competes with high through traffic volumes, resulting in substantial weaving and merging activity.
- Vehicle trips using l-5 for local and short distance travel in the project area. Because of the secure military installations, I-5 is the main and essentially only traffic artery through the area for through trips, regional trips and short trips. As a result, several locations have a heavy volume of trips that begin and end within the project limits, competing for freeway space with regional and through traffic. Further information about these trip patterns can be found in the I-5 JBLM Congestion Relief Study, Travel Patterns and Characteristics report dated August, 2014.


### 3.8 Intersection Analyses at the Reconfigured and Other Area Interchanges on I-5

The 2013 intersection analyses at the l-5 interchanges were conducted using Synchro software following the Highway Capacity Manual (HCM) procedures. A summary of the intersection turning movement volumes used for the analysis is contained in Appendix B. The results of these analyses are summarized Table 1. A detailed listing of the No Build Alternative analysis results is located in Appendix C.

The analyses show that during the AM peak hour the following intersections are operating below LOS D:

- I-5 SB Ramps / Berkeley Street
- I-5 SB Ramps / Thorne Lane
- I-5 NB Ramps/ Thorne Lane

During the PM peak hour, the following intersections operate below LOS D:

- I-5 NB Ramps / Thorne Lane
- I-5 NB Ramps / Center Drive
- I-5 NB Ramps / Gravelly Lake Drive

As interim measures to address these deficiencies, WSDOT and the City of Lakewood have implemented several improvements. In 2014, WSDOT added an auxiliary lane on southbound I-5 between Thorne Lane and Berkeley Street, as well as ramp meters in 2015 to improve operations along l-5 and at the interchanges. The City of Lakewood is planning for an additional improvement at Berkeley Street, as part of the Madigan Access Improvement Project, which will open in 2017 to address the Berkeley Street Interchange deficiencies.

The cloverleaf configuration of the Main Gate interchange does not have traditional intersections with traffic control devices, such as stop signs or traffic signals. To analyze the merge and diverge points on 41st Division Drive with the various l-5 ramps, output from the Meso Model was used to estimate average approach delays. A summary of these approach delays is shown in Table 2.

Based on a review of the estimated approach delays at the l-5 northbound ramps, the northbound approach along 41st Division Drive has an average delay of over five minutes per vehicle during the PM peak hour. The other approaches have delays of less than 30 seconds per vehicle. At the I-5 southbound ramps, the southbound approach along 41st Division Drive has an average delay of over three minutes per vehicle during the PM peak hour. The other approaches have delays of less than 30 seconds per vehicle. These long delays are caused by traffic congestion along the l-5 mainline, which backs up traffic on the on-ramps to their junction with 41st Division Drive.

Table 1: Summary of Interchange Delay and Level of Service (LOS) at the Reconfigured Interchanges and Other Area Interchanges

| Reconfigured Interchanges Existing 2013 |  |  | Other Area Interchanges Existing 2013 |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Intersections | AM | PM | Intersections | AM | PM |
| I-5 NB Ramps/Berkeley Street (Signal) |  |  | I-5 NB Ramps/Center Drive** (2-way Stop) |  |  |
| Average Delay (sec) / LOS | 25.7/C | 29.7/C | Average Delay (sec) / LOS | NA | 40.8/E |
| I-5 SB Ramps/Berkeley Street (Signal) |  |  | l-5 SB Ramps/Center Drive (2-way Stop) |  |  |
| Average Delay (sec) / LOS | 69.2/E | 54.0/D | Average Delay (sec) / LOS | 13.9/B | 12.7/B |
| Berkeley St/Union Avenue (Signal) |  |  | Center Drive/Wilmington Drive (2-way Stop) |  |  |
| Average Delay (sec) / LOS | 10.6/B | 12.1/B | Average Delay (sec) / LOS | 13.0/B | 14.7/B |
| I-5 NB Ramps/Thorne Lane (Signal) |  |  | I-5 NB Ramps/Steilacoom-DuPont Road (2-way Stop) |  |  |
| Average Delay (sec) / LOS | 56.9/E | 71.2/E | Average Delay (sec) / LOS | 32.3/C | 49.9/D |
| l-5 SB Ramps/Thorne Lane (Signal) |  |  | I-5 SB Ramps/Steilacoom-DuPont Road (Signal) |  |  |
| Average Delay (sec) / LOS | 58.7/E | 49.1/D | Average Delay (sec) / LOS | 18.8/B | 27.3/C |
| Thorne Lane/Union Avenue (4-way Stop) |  |  | Steilacoom-DuPont Road/Barksdale Avenue/ Wilmington Drive (Signal) |  |  |
| Average Delay (sec) / LOS | 9.6/A | 11.1/B | Average Delay (sec) / LOS | 43.1/D | 29.7/C |
| NOTES: <br> * - LOS values below "D" shown in bold font <br> ** - Assumes new configuration of intersection built in 2015 |  |  | I-5 NB Ramps/Gravelly Lake Drive (2-way Stop) |  |  |
|  |  |  | Average Delay (sec) / LOS | 39.8/D | 70.3/E |
|  |  |  | I-5 SB Ramps/Gravelly Lake Drive (Signal) |  |  |
|  |  |  | Average Delay (sec) / LOS | 41.9/D | 47.3/D |
|  |  |  | Gravelly Lake Drive/Pacific | way (Sign |  |
|  |  |  | Average Delay (sec) / LOS | 25.5/C | 29.0/C |

Table 2: 2013 Delay Summary at Main Gate Interchange

|  | NB I-5 Ramp / 41 <br> st <br> Drive | Division | SB I-5 Ramp / 41 ${ }^{\text {st }}$ Division Drive |  |
| :--- | :---: | :---: | :---: | :---: |
| Approach | Volume AM/PM | Delay (seconds per <br> vehicle) AM/PM | Volume AM/PM | Delay (seconds per <br> vehicle) AM/PM |
| NB on 41 ${ }^{\text {st }}$ Division Drive | $790 / 1,830$ | $0.1 / 311$ | $690 / 1,445$ | $0.6 / 24.2$ |
| SB on 41 ${ }^{\text {st }}$ Division Drive | $1,335 / 1,195$ | $0.4 / 26.1$ | $1,095 / 1,375$ | $1.1 / 188$ |
| EB on I-5 NB Off-ramp | $285 / 120$ | $0.0 / 0.0$ | $420 / 225$ | $0.9 / 23.4$ |
| WB on I-5 NB Loop Off-ramp | $200 / 60$ | $0.1 / 12.2$ | $240 / 180$ | $0.2 / 0.0$ |

Note: Delay based on Mesoscopic Model Output

### 3.9 Summary of Existing I-5 Traffic Conditions in the JBLM vicinity

A summary of the key findings from the traffic operation analyses of the $2013 \mathrm{l}-5$ conditions includes:

- Traffic volumes along several sections of I-5 in the JBLM area are near or exceed the practical capacity of the highway.
- Travel speeds along several sections of I-5 are below 70 percent of the posted speed (LOS F) with some sections operating between 20 mph to 30 mph .
- These lower travel speeds also reduce the capacity of the l-5 corridor.
- Congestion along the l-5 corridor through the JBLM area can last 2 to 3.5 hours during the PM peak period.
- High levels of exiting and entering traffic from multiple, close-proximity ramps cause drivers to shift lanes frequently, resulting in slow travel speeds.
- The lack of reasonable alternative routes results in short, local trips on I-5 for travel between JBLM and local communities, and between land-locked neighborhoods and other nearby destinations.
- Approximately 12 percent of the drivers wishing to use I-5 cannot use it during the PM peak hour and must travel at other times.
- Several of the ramp terminal intersections currently operate below LOS D.


### 4.0 Future Year Transportation System Assumptions

Over the next 25 years, traffic along the I-5 corridor through the JBLM area is expected to grow and congestion to increase as speeds along l-5 slow. To address this expected growth, WSDOT and local agencies have developed their transportation plans and have selected short-term improvement projects planned for implementation over the next six years. The 2020 and 2040 NoBuild transportation system includes the existing transportation network plus these funded projects, outlined in the local agencies' Transportation Improvement Plans (TIPs) and WSDOT's State Transportation Improvement Plan (STIP), as well as funded JBLM improvements. These highway improvements, located in or near the study area, include:

- I-5 Congestion Management TIGER III: Southbound auxiliary lanes from Thorne Lane to Berkeley Street.
- I-5 Congestion Management TIGER III: Ramp metering, traffic cameras, and variable message signs (See Figure 12).
- Point Defiance Bypass Rail project improvements1.

[^0]- Madigan Gate Access Improvements (See Figure 13).
- Center Drive northbound ramp intersection improvements.
- Joint-Base Connector Phase 1 improvements, including the closure of the Rainer Gate.
- Integrity Gate and Mounts Gate opened with full access and closed the I-Street Gate.

Figure 13: Interim Improvements Using Federal Grant Funding


Figure 12: Access Improvements to Madigan Gate


### 5.0 Traffic Forecasting Modeling Process and Assumptions

The travel forecasts for the l-5 JBLM Vicinity Congestion Relief Study were developed using a series of inter-related and complimentary modeling tools that included a Macroscopic (Macro) Model, Mesoscopic (Meso) Model and Transit Sketch Planning (Transit) Model. Each of the three modeling tools was developed specifically for the I-5 JBLM Vicinity Congestion Relief Study and were used to evaluate the No Build and Build Alternatives. More extensive information is available in that study, while the following is a general description of each model and how they were integrated for the project.

### 5.1 Macroscopic Model

The I-5 JBLM Macro Model was used to develop travel forecasts in the study area and to understand travel pattern changes that would result from various improvement alternatives. The Macro Model has a base year of 2013, and two forecast horizon years of 2020 (opening year) and 2040 (design year). The model area includes Pierce County south of the Puyallup River and northern Thurston County. The model includes trip assignments for both high-occupancy vehicle (HOV) and single-occupancy vehicle (SOV) mode splits for two time periods: AM peak period (6 AM to 9 AM), and PM peak period (3 PM to 6 PM). The Macro Model is consistent with local land use plans, and the Puget Sound Regional Council (PSRC) and Thurston Regional Planning Council (TRPC) regional models.

### 5.2 Transit Sketch Planning Model

The Transit Model was developed to provide a more comprehensive, multimodal assessment of how corridor level improvements can help achieve the congestion reduction goals of the project. The Transit Model captured the effects that commuter-oriented transportation demand management programs (subsidized transit passes, vanpools, shuttles, etc.), investments in highoccupancy vehicle facilities, and improvements to commuter transit service can have on congestion in the corridor. Using the Transit Model in the planning process also allowed the project team to better understand the commuter transit market in this corridor.

The Transit Model was designed to build on the existing Macro Model while also integrating with the Meso Model. The Transit Model used data from the established regional models, as well as data that had been identified through industry research as important for forecasting commuter transit ridership.

The Transit Model was integrated into the overall modeling process, interfacing directly with the Macro Model. A variety of data inputs from the Macro Model fed into the Transit Model including SOV and HOV travel times. Once transit ridership forecasts for each alternative were developed, the data were input back into the Macro Model to account for the changes in mode share.

Ridership forecasts were also used directly in performance assessments of the improvement alternatives.

### 5.3 Mesoscopic Model

The I-5 JBLM Meso Model was developed to evaluate a series of detailed transportation performance measures that could be used to compare each of the improvement alternatives. The Meso Model was built using Dynameq software and is based upon the Macro Model, so it is also consistent with local and regional land use plans and regional transportation models. The general analysis area of the Meso Model is the I-5 corridor between SR 512 and SR 510, including the adjoining local on-JBLM and off-JBLM arterials. The Meso Model incorporates specific roadway and intersection operational details, such as signal timing, roadway channelization, ramp metering, and merging/weaving conflicts along the l-5 mainline. It also includes operational impacts from at-grade railroad crossings and military gate operations. These features enable the Meso Model to dynamically balance traffic volumes as the various alternative routes become congested.

The Meso Model has a base year of 2013 and two forecast horizon years of 2020 and 2040. The model includes trip assignments for both high-occupancy vehicle (HOV) and single-occupancy vehicle (SOV) modes for two time periods: AM peak period (5 AM to 11 AM) and PM peak period (2 PM to 8 PM). The 6-hour time periods provide the opportunity to evaluate impacts from increased congestion and peak spreading already occurring along the l-5 corridor.

### 5.4 Modeling Procedure

Outputs from the modeling effort were coordinated between the three different models. Figure 14 illustrates the general procedure for modeling each alternative. Step 1 included coding the Macro Model with the assumptions inherent in the improvement alternative, running the model, and outputting SOV and HOV travel time trip tables for use in the Transit Sketch Model. Step 2 included coding the Transit Sketch Model with the improvement alternative's assumptions, running the model, and outputting transit ridership and vehicle trip adjustments (changes in amount of vehicle trips due to changes in transit ridership) for use back in the Macro Model. Step 3 included revising the Macro Model with the transit ridership adjustments, re-running the model, and outputting vehicle volume metrics and subarea trip tables for use in the Meso Model. The final step, Step 4, included detailed operational coding of the Meso Model, running the model, and then outputting various performance metrics, such as travel volumes, speeds, times and hours of congestion and mode shares.

Figure 14: Model Process Flowchart

## Outputs



### 6.0 2020 and 2040 I-5 No Build Alternative Traffic Analysis

The following section summarizes the base traffic operations along l-5 for an opening year (2020) and a design year (2040) time frame. Synchro software is used to analyze signalized and nonsignalized intersections; Sidra software is used to analyze roundabout operations; and SimTraffic and the Meso Model are used to simulate and analyze traffic operations along the I-5 mainline and at interchanges.

### 6.1 Future No Build Alternative I-5 Traffic Volumes

The forecasted No Build Alternative traffic volumes along I-5 for both the AM and PM peak hours, are shown in Figures 15 and 16, respectively. In 2020, the two-way traffic volume along I-5 between Center Drive and Gravelly Lake Drive ranges from approximately 8,200 to nearly 11,000 vehicle trips in the AM peak hour and from 7,400 to nearly 11,000 vehicle trips in the PM peak hour. In 2040, the two-way traffic volume along l-5 ranges from approximately 8,600 to 11,200 vehicle trips in the AM peak hour and from 7,200 to nearly 10,100 vehicle trips in the PM peak hour.

Figure 15: 2020 and 2040 AM Peak Hour Volumes on I-5 - No Build Alternative
AM Peak Hour Volume along 1-5-2020
Center Drive to Gravelly Lake Drive


AM Peak Hour Volume along I-5-2040
Center Drive to Gravelly Lake Drive


Figure 16: 2020 and 2040 PM Peak Hour Volumes on I-5 - No Build Alternative
PM Peak Hour Volume along 1-5-2020 Center Drive to Gravelly Lake Drive


PM Peak Hour Volume along 1-5-2040 Center Drive to Gravelly Lake Drive


The lower number of PM vehicle trips along I-5 as compared to the AM vehicle trips is because of the slower travel speeds in the PM which reduces the number of vehicles than can actually use the I-5 corridor during the PM peak hour. The small growth in vehicle trips along l-5 between 2020 and 2040 in the AM peak hour and the decrease in vehicle trips in the PM peak hour are also because of the reduction in average travel speeds, caused by the increased congestion, resulting in trips being diverted to other travel departure times.

### 6.2 Average Daily Traffic along the I-5 Mainline

Using the 2020 and 2040 land use assumptions, the travel demand/operational modeling tools were used to estimate Average Daily Traffic (ADT) and peak period volumes for 2020 and 2040 with the No Build and Build Alternatives. A summary of the estimated daily traffic growth on I-5 from the Center Drive interchange and the Gravelly Lake Drive interchange is shown in Table 3. Due to the congestion along l-5 and the reduced number of travel lanes south of Thorne Lane, the No Build Alternative would attract fewer vehicles to the corridor and results in lower growth than the Build Alternative that includes added capacity. Depending on location, existing traffic volumes are projected to increase by approximately 0.8 percent to 1.4 percent per year over the long-range planning horizon (2040). A detailed summary of peak hour and ADT volumes in listed in Appendix D.

Table 3: Daily Traffic Growth on I-5 in the JBLM Vicinity

|  | 2-Way Average Daily Traffic Volumes on I-5 in Vicinity of JBLM |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Scenario |  |  |  |  |  |  |  |  |  | $\begin{aligned} & 0 \\ & \stackrel{0}{0} \\ & \mathbf{0} \\ & 0 \\ & \mathbf{c} \\ & 0 \\ & 1 \end{aligned}$ |  |  |  |
| $2013$ <br> Existing | 122,000 |  | 124,000 |  | 120,000 |  | 129,000 |  | 137,000 |  | 146,000 |  | 143,000 |
| $2020$ <br> No Build | 135,900 |  | 132,600 |  | 130,000 |  | 138,000 |  | 149,700 |  | 159,100 |  | 154,900 |
| 2020 <br> Build Alt | 135,700 |  | 137,300 |  | 141,800 |  | 154,400 |  | 168.900 |  | 167.300 |  | 158,800 |
| 2040 <br> No Build | 164,600 |  | 152,700 |  | 149,600 |  | 154,200 |  | 165,800 |  | 181,800 |  | 171,100 |
| $2040$ <br> Build Alt | 165,600 |  | 158,900 |  | 170,100 |  | 183,900 |  | 195,0 00 |  | 192.000 |  | 176,600 |

### 6.3 2020 and 2040 No Build Alternative Travel Demand along I-5

In 2013, 99 percent of the AM peak hour demand for travel on I-5 was accommodated and just over 88 percent of the PM peak hour was able to operate on I-5, based on person miles of travel from the Meso Model. By 2020, the ability of the No Build Alternative to meet AM peak hour
demand is expected to about 94 percent, and by 2040 it would continue to drop to about 74 percent. During the PM peak hour, the travel demand that could be accommodated on I-5 with the No Build Alternative is forecast to drop to about 71 percent in in 2020, and to about 30 percent by 2040. Increased congestion along I-5 through the JBLM area prevents drivers who want to travel on I-5 from using it during peak travel times.

The traffic volume forecasts discussed in the preceding paragraphs and highlighted in Table 3 represent expectations of the level of traffic that would use l-5 in the study area in 2020 and 2040. This differs from the level of traffic that would like to use the corridor during these time periods. A key performance measure for understanding the impact of congestion on the l-5 corridor involves assessing the amount of travel demand that could be accommodated during the PM (highest) peak hour. This subsection discusses the ability of the No Build and Build Alternatives to meet demand for travel in the corridor in 2013, 2020 and 2040.

PM Peak Hour - As shown in Figure 17, the level of demand for travel on I-5 during the PM peak hour is substantively higher than what could actually be accommodated with either the No Build or Build Alternatives. As indicated by the data in this figure, the No Build Alternative would accommodate less travel demand on I-5 than 2013 conditions during the PM peak hour. In 2020, the No Build Alternative would accommodate approximately 70 percent of demand, while in 2013 slightly more than 88 percent of demand was met. By 2040, the No Build Alternative would accommodate about 30 percent of the PM peak hour demand. This finding is a useful indicator of the duration of congestion which would not only affect the PM peak hour, but would likely spread into the hours adjacent to the peak. The greater the percentage of travel demand that cannot be met in a single peak hour, the greater the total number of hours of peak period congestion that would be expected.

Figure 17: 2020 and 2040 Met and Unmet Travel Demand on I-5 during PM Peak Hour


PM Peak Three Hours - While over 88 percent of existing demand during the single 2013 PM peak hour can be accommodated in the corridor, Figure 16 shows that nearly everyone who wanted to travel on l-5 in 2013 could make the journey at some point during the three hour PM peak period. Only one percent of all PM peak three hour demand could not be satisfied during this time period. Figure 18 also shows that as demand grows to 2020, over 90 percent of demand could be accommodated with the No Build Alternative. By 2040, less than 72 percent of demand could be accommodated by the No Build Alternative during the three-hour PM peak period.

Figure 18: 2020 and 2040 Met and Unmet Demand on I-5 during PM Peak 3-hours



2020
2020 Demand on l-5 Met during 3-hour PM Peak Period No Build Alternative
*Demand based on person miles of travel estimate from Mesoscopic travel model.

### 6.4 Average 2020 and 2040 I-5 Travel Speeds

Predicted average travel speeds along the I-5 corridor in 2020 and 2040 for the AM peak hour are illustrated in Figure 19. As can be observed from the figure, 2020 and 2040 AM peak hour northbound travel speeds along l-5 would be around the posted speed of 60 mph north of Center Drive. In the southbound direction, travel speeds are expected to fall below 42 mph or LOS F north of Thorne Lane. These slow speeds would be attributed to the reduction in the number of travel lanes from four lanes to three lanes, requiring drivers to merge. This slows traffic and causes backups north of this choke point.

Figure 20 illustrates expected travel speeds during the 2020 and 2040 PM peak hours. As shown in this figure, 2020 and 2040 PM peak hour northbound travel speeds would be below 42 mph or LOS F, with some sections below 10 mph . The only exception is north of Thorne Lane where speeds are
expected to return to near the posted speed limit, because the number of travel lanes increase from three to four lanes. Figure 21 presents projected PM peak hour travel speeds visually.

Figure 19: 2020 and 2040 AM Peak Hour Average Travel Speeds on I-5 - No Build Alternative

AM Peak Hour Travel Speeds along 1-5-2020 Center Drive to Gravelly Lake Drive


AM peak Hour Travel Speeds along 1-5-2040
Center Drive to Gravelly Lake Drive


Figure 20: 2020 and 2040 PM Peak Hour Average Travel Speeds on I-5 - No Build Alternative

PM Peak Hour Travel Speeds along 1-5-2020
Center Drive to Gravelly Lake Drive


PM Peak Hour Travel Speeds along 1-5-2040 Center Drive to Gravelly Lake Drive


Figure 21: 2020 and 2040 PM Peak Hour Travel Speeds on I-5 between Center Drive and Gravelly Lake Drive - No Build Alternative


In the southbound direction during 2020, PM peak hour travel speeds would be generally below 42 mph or LOS F, except for a short section between Steilacoom-DuPont Road and Center Drive where traffic speeds are expected to increase to around 50 mph as traffic volumes stabilize. During 2040 southbound travel speeds on I-5 between Gravelly Lake Drive and Center Drive are expected to be less than 30 mph with some sections at 10 mph or below. These slow average PM speeds signify severe congestion with slow moving vehicles and periods of stop-and-go traffic.

### 6.5 2020 and 2040 Hours of Congestion along I-5

Based on the Mesoscopic Model data, estimates were made of the number of hours the travel speed operated below 70 percent of posted speed or 42 mph in 2020 and 2040. Based on the analysis, less than one hour of congestion north of Thorne Lane is expected to occur southbound during the AM peak period in 2020. By 2040, the congestion north of Thorne Lane is expected to increase to 3.5 hours during the AM peak period.

During the PM peak period in 2020 and 2040, several hours of congestion occur along l-5 between Center Drive and Gravelly Lake Drive, as illustrated in Figure 22. These hours of congestion could last around four hours in 2020 and over five hours by 2040 in both the northbound and southbound directions.

The travel speed diagrams, illustrated in Figure 23, show that these slow average speeds and hours of congestions during the PM peak period extend between 2:00 PM and 8:00 PM and beyond. These diagrams show that there are several areas that speeds fall below 42 mph . In 2020, the southbound congestion generally extends north of the Main Gate Interchange with some congestion associated with the heavy on-ramp traffic at Center Drive. The northbound congestion in 2020 is south of Thorne Lane where the number of travel lanes increase from three lanes to four lanes. By 2040, congestion extends past the 8:00 PM analysis period and would geographically extend both north and south of the study area.

### 6.6 2020 and 2040 On- and Off-Ramp No Build Alternative Volumes along I-5

On- and Off-ramp volumes along l-5 between Center Drive and Gravelly Lake Drive remain high in 2020 and 2040. A comparison of the 2020 and 2040 AM peak hour on- and off-ramp volumes is shown in Figure 24. Overall, ramp volumes generally decrease in 2040 over the 2020 volumes during the peak hour because of increased congestion along l-5.

Similarly, in 2040 AM peak hour, there are about 3,660 vehicles exiting I-5 and 2,070 vehicles entering l-5 at these seven interchanges southbound and about 3,450 vehicles exiting l-5 and 3,040 vehicles entering l-5 northbound. Again, the total of trips entering and exiting l-5 continues to be more than the capacity of a single lane, requiring drivers to shift lanes.

Figure 22: Hours of Congestion on I-5 during 2020 and 2040 PM Peak Periods from Center Drive to Gravelly Lake Drive - No Build Alternative

PM Peak Period - Hours of Congestion along l-5-2020 Center Drive to Gravelly Lake Drive


PM Peak Period - Hours of Congestion along l-5-2040 Center Drive to Gravelly Lake Drive


Figure 23: Travel Speeds on I-5 during the 2020 and 2040 PM Peak Period - No Build Alternative


A comparison of the PM peak hour on- and off-ramp volumes in 2020 and 2040 is shown in Figure 25. Overall at the six interchanges along l-5 in the study area in 2020, there are a total of about 2,300 vehicles exiting I-5 and 4,370 vehicles entering I-5 southbound, and about 2,640 vehicles exiting l-5 and 4,760 vehicles entering l-5 northbound.

Figure 24: 2020 and 2040 AM On- and Off-Ramp Volumes on I-5 from Center Drive to Gravelly Lake Drive - No Build Alternative

2020 AM Peak Hour On and Off-Ramp Volumes along I-5 Center Drive to Gravelly Lake Drive


- 2020 SB

■ 2020 NB

2040 AM Peak Hour On and Off-Ramp Volumes along I-5 Center Drive to Gravelly Lake Drive


■ 2040 SB
■ 2040 NB

Figure 25: 2020 and 2040 PM On- and Off-Ramp Volumes on I-5 from Center Drive to Gravelly Lake Drive - No Build Alternative

2020 PM Peak Hour On and Off-Ramp Volumes along I-5 Center Drive to Gravelly Lake Drive


2040 PM Peak Hour On and Off-Ramp Volumes along I-5
Center Drive to Gravelly Lake Drive


Similarly, in 2040 during the PM peak hour, there are about 2,210 vehicles exiting l-5 and 4,500 vehicles entering l-5 at these six interchanges southbound and about 2,220 vehicles exiting l-5 and 4,740 vehicles entering $1-5$ at these six interchanges northbound

All of this traffic cannot be in the outside lane at the same time, so drivers frequently change lanes to enter and exit l-5. This heavy amount of lane change movement causes traffic to slow, increases congestion, and reduces the overall traffic throughput in the JBLM area.

### 6.7 Comparison of I-5 No Build Alternative Travel Times

A comparison of No Build Alternative travel times along I-5 between Center Drive and Gravelly Lake Drive was made using output from the Meso Model. As shown on Figure 26, drivers traveling southbound on I-5 during the AM peak period would generally operate near or at the posted speed limit in 2013 and 2020 and take about nine minutes. By 2040, southbound travel time would increase to about 12 minutes in the northbound direction in 2013, drivers operated about the posted speed and take around 8.1 minutes to travel between Center Drive and Gravelly Lake Drive. In both 2020 and 2040, the No Build Alternative northbound travel time would increase to about nine minutes during the AM peak hour.

During the PM peak period, 2013 southbound travel times along l-5 between Center Drive and Gravelly Lake Drive were estimated at about 15 minutes with no accidents, while in the northbound direction, it would take drivers about 12 minutes. By 2020, No Build Alternative southbound PM travel times are expected to increase to around 37 minutes, while it would take northbound drivers about 26 minutes to travel between Center Drive and Gravelly Lake Drive.

Figure 27 plots the travel time data in the northbound direction. In the northbound direction, 2040 No Build Alternative PM peak hour travel times are expected to increase to about 34 minutes between Center Drive and Gravelly Lake Drive. In the southbound direction, 2040 No Build Alternative PM peak hour travel times are expected to increase to about 48 minutes during the peak hour. The southbound 2040 PM Peak hour travel time between Thorne Lane and Main Gate is expected to be slightly better than the 2020 travel time because of a bottleneck at SR 512 which is limiting the amount of traffic that can travel southbound in 2040 and allows some drivers to temporarily speed up in this area. In 2020, the SR 512 bottleneck is less restrictive than in 2040 so more traffic can get through which reduces travel speeds between Thorne Lane and Main Gate.

Figure 26: Comparison of Southbound Cumulative Travel Times during AM and PM Peak Hours No Build Alternative

## Comparison of No Build AM Peak Hour Cum ulative Travel Times along Southbound l-5 from Gravelly Lake Drive to Center Drive



Comparison of No Build PM Peak Hour Cumulative Travel Times along Southbound l-5 from Gravelly Lake Drive to Center Drive


Figure 27: Comparison of Northbound Cumulative Travel Times during AM and PM Peak Hours No Build Alternative

Comparison of No Build AM Peak Hour Cumulative Travel Times along Northbound I-5 from Center Drive to Gravelly Lake Drive


Comparison of No Build PM Peak Hour Cumulative Travel Times along Northbound l-5 from Center Drive to Gravelly Lake Drive


### 6.8 Summary of Future Year Intersection Analysis with the No Build Alternative at the Reconfigured and Adjacent Interchanges along I-5

The future year intersection analyses at the l-5 interchanges with the No Build Alternative assumed that the following intersection and mainline improvements were implemented:

- A southbound auxiliary lane was added between the Thorne Lane on-ramp to the Berkeley Street off-ramp
- Ramp meters were added to the on-ramps at all interchanges except the northbound Thorne Lane ramp
- The Madigan Access improvements at the Berkeley Street Interchange were implemented, including a second left-turn lane on the southbound off-ramp, a second lane on the Berkeley Street bridge easterly towards JBLM, and a third lane on Murray Road from the northbound off-ramps into JBLM.
- I-5 northbound ramp intersection with Center Drive was improved to better tie the exit from JBLM into the intersection.

The intersection analyses were conducted using Synchro software following the Highway Capacity Manual procedures. The results of these analyses for the two Build Alternative interchanges are summarized in Table 4. The analyses show that during the AM and PM peak hours, intersections at the Thorne Lane Interchange would operate at LOS D or better in both 2020 and 2040. The interim Madigan Access Improvements would allow the Berkeley Street Interchange to operate at LOS D or better in 2020 and 2040.

The results of the intersection analyses for the adjacent interchanges at Center Drive, SteilacoomDuPont Road, and Gravelly Lake Drive are summarized in Table 5. The analyses show that the ramp intersections at Center Drive, Steilacoom-DuPont Road, and at Gravelly Lake Drive would operate at LOS D or better during the 2020 AM and PM peak hours. In 2040 the southbound ramp intersections at Center Drive and Steilacoom-DuPont Road would operate at LOS E during the AM peak hour. During the 2040 PM peak hour the intersections of the northbound and southbound ramps at Steilacoom-DuPont Road and at Gravelly Lake Drive are expected to be at or below LOS D.

In reviewing these results, it is important to remember the following data constraints:

- Congestion along I-5 limits the amount of traffic wanting to use I-5, as indicated in the previous section (only 30 percent of the demand that wants to use I-5 during the 2040 PM peak hour can actually use I-5). This reduces the amount of traffic at the various intersections.
- The Synchro analyses do not account for queue back-ups on the on-ramps from the ramp meters or queues from l-5 congestion into the intersection.

A list of the turning movements used for both the Synchro analyses and from the mesoscopic model is shown in Appendix B. A more detailed summary of the intersection analyses is contained in Appendix C .

Table 4: Summary of Interchange Delay and Level of Service (LOS) at the Reconfigured Interchanges - No Build Alternative

| Intersection ${ }^{2}$ | 2013 Existing |  | 2020 No Build ${ }^{3}$ |  | 2040 No Build ${ }^{3}$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | AM | PM | AM | PM | AM | PM |
| I-5 NB Ramps / Berkeley Street ${ }^{3}$ |  |  |  |  |  |  |
| Control Type | Signal |  | Signal |  | Signal |  |
| Average Delay (sec) / LOS | 25.7/C | 29.7/C | 16.3/B | 20.8/C | 11.4/B | 14.5/B |
| I-5 SB Ramps / Berkeley Street ${ }^{3}$ |  |  |  |  |  |  |
| Control Type | Signal |  | Signal |  | Signal |  |
| Average Delay (sec) / LOS | 69.2/E | 54.0/D | 36.0/D | 26.0/C | 32.4/C | 23.8/C |
| Berkeley Street / Union Avenue |  |  |  |  |  |  |
| Control Type | All-way Stop |  | Signal |  | Signal |  |
| Average Delay (sec) / LOS | 10.6/B | 12.1/B | 11.0/B | 12.0/B | 10.0/B | 12.7/B |
| Berkeley Street / Washington Ave |  |  |  |  |  |  |
| Control Type | 2-way Stop |  | 2-way Stop |  | 2-way Stop |  |
| Average Delay (sec) / LOS | NA | NA | 12.6/B | 14.3/B | 14.2/B | 12.2/B |
| I-5 NB Ramps / Thorne Lane |  |  |  |  |  |  |
| Control Type | Signal |  | Signal |  | Signal |  |
| Average Delay (sec) / LOS | 56.9/E | 71.2/E | 34.2/C | 37.9/D | 37.3/D | 36.6/D |
| I-5 SB Ramps / Thorne Lane |  |  |  |  |  |  |
| Control Type | Signal |  | Signal |  | Signal |  |
| Average Delay (sec) / LOS | 58.7/E | 49.1/D | 33.9/C | 47.5/D | 49.5/D | 44.4/D |
| Thorne Lane / Union Avenue |  |  |  |  |  |  |
| Control Type | 2-way Stop |  | 2-way Stop |  | 2-way Stop |  |
| Average Delay (sec) / LOS | 9.6/A | 11.1/B | 10.4/B | 11.6/B | 11.2/B | 12.8/B |

Notes ${ }^{1}$ LOS values less than "D" shown in bold font
${ }^{2}$ Signalized \& non-signalized intersections analyzed using Synchro software. Please note that the Synchro analysis does not account for back-ups on on-ramp from the ramp meter or freeway.
${ }^{3}$ Assumes Madigan Access Improvements at the Berkeley Street Interchange are implemented by 2020

Table 5: Summary of Interchange Delay and Level of Service (LOS) at other Area Interchanges No Build Alternative

| Intersection ${ }^{2}$ | 2013 Existing |  | 2020 No Build |  | 2040 No Build |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | AM | PM | AM | PM | AM | PM |
| I-5 NB Ramps / Center Drive ${ }^{3}$ |  |  |  |  |  |  |
| Control Type | 2-way Stop |  | 2-way Stop |  | 2-way Stop |  |
| Average Delay (sec) / LOS | NA | 40.8/E | 12.3/B | 12.7/B | 12.0/B | 11.9/B |
| I-5 SB Ramps / Center Drive |  |  |  |  |  |  |
| Control Type | 2-way Stop |  | 2-way Stop |  | 2-way Stop |  |
| Average Delay (sec) / LOS | 13.9/B | 12.7/B | 18.6/C | 13.3/B | 35.1/E | 13.2/B |
| Center Drive / Wilmington Drive |  |  |  |  |  |  |
| Control Type | Signal |  | Signal |  | Signal |  |
| Average Delay (sec) / LOS | 13.0/B | 14.7/B | 14.1/B | 20.2/C | 18.4/B | 20.2/C |
| I-5 NB Ramps / Steilacoom-DuPont Road |  |  |  |  |  |  |
| Control Type | Signal |  | Signal |  | Signal |  |
| Average Delay (sec) / LOS | 32.3/C | 49.9/D | 22.5/C | 45.1/D | 29.7/C | 57.9/E |
| I-5 SB Ramps / Steilacoom-DuPont Road |  |  |  |  |  |  |
| Control Type | Signal |  | Signal |  | Signal |  |
| Average Delay (sec) / LOS | 18.8/B | 27.3/C | 34.0/C | 29.1/C | 68.7/E | 37.5/D |
| Steilacoom-DuPont Road / Barksdale Avenue / Wilmington Drive |  |  |  |  |  |  |
| Control Type | Signal |  | Signal |  | Signal |  |
| Average Delay (sec) / LOS | 43.1/D | 29.7/C | 36.9/D | 27.1/C | 58.2/E | 26.6/C |
| I-5 NB Ramps / Gravelly Lake Drive |  |  |  |  |  |  |
| Control Type | Signal |  | Signal |  | Signal |  |
| Average Delay (sec) / LOS | 39.8/D | 70.3/E | 46.5/D | 41.6/D | 35.4/D | 49.6/D |
| I-5 SB Ramps / Gravelly Lake Drive |  |  |  |  |  |  |
| Control Type | Signal |  | Signal |  | Signal |  |
| Average Delay (sec) / LOS | 41.9/D | 47.3/D | 31.3/C | 37.2/D | 32.8/C | 40.8/D |
| Gravelly Lake Drive / Pacific Highway |  |  |  |  |  |  |
| Control Type | Signal |  | Signal |  | Signal |  |
| Average Delay (sec) / LOS | 25.5/C | 29.0/C | 32.0/C | 37.1/D | 34.6/C | 34.7/C |

Notes ${ }^{1}$ LOS values less than " $D$ " shown in bold font
${ }^{2}$ Signalized \& non-signalized intersections analyzed using Synchro software. Please note that the Synchro analysis does not account for back-ups on on-ramp from the ramp meter or freeway.
${ }^{3}$ The I-5 NB Ramps / Center Drive intersection was redesigned in 2015. This new design is reflected in the 2020 and 2040 analysis.

### 7.0 Description of the Build Alternative

Based on the analysis conducted in the Corridor Plan Feasibility Study, the Multimodal Alternatives Analysis, and the preliminary corridor traffic analysis, the most promising alternative was selected for further environmental analysis as part of the NEPA assessment and the I-5 JBLM Vicinity Interchange Justification Report (IJR). The Corridor Plan Feasibility Study, the Multimodal Alternatives Analysis, and a description of the alternative packages considered are included in Appendix E. The Build Alternative includes the following elements, as illustrated in Figure 28:

- Mainline widening adds a fourth lane northbound on I-5 from the Steilacoom-DuPont Road interchange on-ramp to Thorne Lane interchange, and southbound from Thorne Lane to Center Drive. The new lanes would operate for General Purpose (GP) traffic. See Figure 28 for an illustration of the added travel lanes.
- Auxiliary lanes would be added northbound between the Berkeley Street and Thorne Lane interchanges and between the Thorne Lane and Gravelly Lake Drive interchanges. The existing southbound auxiliary lanes would be maintained between Thorne Lane and Berkeley Street and between Center Drive and Mounts Road. The existing northbound auxiliary lane between Center Drive and Steilacoom-DuPont Road would also be maintained. See Figure 29 for the location of existing and proposed auxiliary lanes.
- Interchange reconfigurations are included at Thorne Lane and at Berkeley Street:
- The Thorne Lane Interchange would be relocated approximately 350 feet south of the existing Thorne Lane Bridge and reconfigured as a tight diamond interchange with roundabouts at the ramp intersections. It would be elevated to grade separate Thorne Lane over the adjacent rail line and Union Avenue. A new loop road would be added to connect Thorne Lane with Union Avenue. A preliminary rendering of the relocated Thorne Lane Interchange is illustrated in Figure 30.
- The Berkeley Street Interchange would be relocated approximately 120 feet south of the existing Berkeley Street Bridge and reconfigured as a tight diamond interchange with roundabouts at the ramp intersections. It would be elevated to grade separate the extension of Jackson Avenue over the adjacent rail line and Militia Drive. The extended Jackson Avenue would loop around an existing business and descend to grade at the intersection of Berkeley Street and Washington Avenue. A preliminary rendering of the relocated Berkeley Street Interchange is also illustrated in Figure 30.
- The relocated interchanges would be designed to accommodate I-5 mainline widening, improve traffic operations at the interchanges, provide pedestrian and bicycle facilities and accommodate planned community growth and support activities at JBLM and Camp Murray through improved access and circulation.


## Figure 28: Proposed Build Alternative



Figure 29: Existing and Proposed I-5 Build Alternative with Average Daily Traffic

EXISTING 2013 CONDITION

1.5 Mainline 2013 ADT and " K " factors
122,000
$1222,000 \quad 124,00$

| 120,000 |
| :---: |
| 0.073 |

129,000
0.663
137,000
$\substack{3006}$

| 146.000 |
| :---: |
| 0.075 |

143,000


Figure 30: Proposed Thorne Lane and Berkeley Street Interchange Concepts


Rendering of the Proposed I-5/Thorne Lane Interchange


Rendering of the Proposed I-5/Berkeley Street Interchange

- Gravelly -Thorne Connector would be constructed to reduce short trips on I-5 between the Tillicum neighborhood and Lakewood. The new connector road would be a single southbound lane parallel and west of the adjacent rail line and extend between Gravelly Lake Drive and Thorne Lane. A preliminary layout for the Gravelly-Thorne Connector is illustrated in Figure 31. The connector would use approximately 25 feet of the railroad right of way and approximately five feet of the golf course right of way. Non-motorized linkages would also be included in its design.

Figure 31: Proposed Gravelley-Thorne Connector

——One Lane Southbound

- Northbound Auxiliary Lane

Proposed Gravelly-Thorne

- Bicycle/Pedestrian Path
- Bicycle/pedestrian shared use path would be added to provide enhanced nonmotorized access along the corridor. A preliminary layout of the bicycle/pedestrian route is illustrated in Figure 32. New sections of the shared used paths are planned along the new Gravelly-Thorne Connector (segment one in the figure), as well as from the new Berkeley Street interchange along the east side of I-5 crossing to the west side just south of Camp Murray and extending to Steilacoom-DuPont Road (segment three). Between Thorne Lane and Berkeley Street (segment two), and between Center Drive and Steilacoom-DuPont Road (segment four), bicycles and pedestrians would use existing local streets and pedestrian facilities in the communities of Tillicum and DuPont.

Figure 32: Recommended Bicycle/Pedestrian Pathway Concept


## $8.0 \quad 2020$ and 2040 I-5 Traffic Analysis for the Build Alternative

The following section summarizes the traffic operations along l-5 for the Build Alternative in the opening year (2020) and in the design year (2040). Synchro software was used to analyze signalized and non-signalized intersections; Sidra software was used to analyze roundabout operations; and SimTraffic and the Meso Model were used to simulate traffic operations.

### 8.12020 and 2040 Build Alternative Average Peak Hour I-5 Traffic Volumes

The forecasted travel volumes along I-5 for the Build Alternative during the AM and PM peak hours are shown in Figures 33 and 34, respectively. In 2020, the two-way traffic volume along I5 between Center Drive and Gravelly Lake Drive would range from approximately 9,200 to nearly 10,900 vehicles in the AM peak hour with an overall average volume of about 10,200 vehicles. During the 2020 PM peak hour, two-way traffic volumes would range from 8,200 to nearly 11,300 vehicles with an overall average of about 9,900 vehicles. These AM peak hour Build Alternative volumes would represent a 6.6 percent increase in vehicles over the 2020 No Build Alternative, and the PM peak hour Build Alternative volumes would be about 12.5 percent higher than 2020 No Build Alternative volumes.

In 2040, the two-way traffic volume along l-5 would range from approximately 10,100 to nearly 13,300 vehicles in the AM peak hour with an overall average two-way volume of 11,700 vehicles. In the 2040 PM peak hour, two-way traffic volumes on I-5 are expected to range from about 7,700 to 11,100 vehicles with an average of about 9,400 vehicles operating along I-5. These AM peak hour Build Alternative volumes would represent an 18.8 percent increase in vehicles over the 2040 No Build Alternative, while PM peak hour Build Alternative volumes would be about 8.8 percent higher than the No Build Alternative.

The lower PM vehicle trips along I-5 in 2040, as compared to the AM vehicle trips are expected to result because the increases congestion would cause lower travel speeds in the PM peak. This would reduce the number of vehicles than can actually use the l-5 corridor during the PM peak hour. The small growth in vehicles along l-5 between 2020 and 2040 in the AM peak hour, and the decrease in vehicle trips in the PM peak hour would result from the reduction in average travel speeds along l-5, caused by increased congestion, and by trips being diverted to other travel times to avoid congestion.

Figure 33: Average 2020 and 2040 AM Peak Hour Volumes on I-5 from Center Drive to Gravelly Lake Drive - Build Alternative



Figure 34: Average 2020 \& 2040 PM Peak Hour Vehicles along I-5 from Center Drive Road to Gravelly Lake Drive - Build Alternative



### 8.2 Travel Demand along l-5 - Build Alternative

PM Peak Hour - As shown in Figure 35, the level of demand for travel on I-5 during the PM peak hour is substantively higher than what could actually be accommodated with either the No Build or Build Alternatives. Additionally, the No Build Alternative could accommodate less travel demand on I-5 than the Build Alternative.

In 2020, the Build Alternative could accommodate a slightly higher percentage of the demand than the 2013 existing system ( 89.2 percent vs. 88.1 percent), and almost 19 percent more ( 89.2 percent vs. 70.5 percent) than the 2020 No Build Alternative. By 2040, the Build Alternative could accommodate about 49 percent of the PM peak hour demand, while the No Build Alternative could accommodate only about 30 percent of the demand. This finding is a useful indicator of the duration of congestion which would not only affect the PM peak hour, but would likely spread into the hours adjacent to the peak. The greater the percentage of travel demand that cannot be met in a single peak hour, the greater the total number of hours of peak period congestion that would be expected.

During the AM peak hour in 2020, it is expected that nearly 99 percent of the demand for travel on I-5 could be accommodated with the Build Alternative. This compares with the 2020 No

Figure 35: 2020 \& 2040 Travel Demand along I-5 during AM and PM Peak Hours from Center Drive to Gravelly Lake Drive - Build Alternative

*Demand based on person miles of travel estimate from Mesoscopic

Build Alternative that could accommodate about seven percent less demand. In 2040, about 90 percent of AM peak hour travel demand on I-5 could be accommodated with the Build Alternative, as compared to the 2040 No Build Alternative which could accommodate about 29 percent less demand. Thus, while congestion would exist, the situation is expected to be substantially better than with the No Build Alternative.

PM Peak Three Hours: While over 88 percent of existing demand during the single 2013 PM peak hour can be accommodated in the corridor, Figure 36 shows that nearly everyone who wanted to travel on I-5 in 2013 could make the journey at some point during the three hour PM peak period. Only one percent of all PM peak three hour demand could not be satisfied during this time period. Figure 36 also shows that as demand grows to 2020, over 90 percent of demand could be accommodated with the No Build Alternative, while nearly 98 percent could be accommodated by the Build Alternative. By 2040, less than 72 percent of demand could be accommodated by the No Build Alternative, while the Build Alternative is expected to accommodate 80 percent of demand during the three-hour PM peak period.

Figure 36: Comparison of 3-Hour PM Peak Period Demand Met on I-5 in the Vicinity of JBLM

*Demand based on person miles of travel estimate from Mesoscopic travel

### 8.3 Future Build Alternative Average Peak Hour I-5 Travel Speeds

Expected average travel speeds along the l-5 corridor in 2020 and 2040 for the AM peak hour and the PM peak hour are illustrated in Figures 37 and 38, respectively. As can be observed from the figures, in both 2020 and 2040 travel speeds along l-5 in the AM peak hour with the proposed improvements range from 50 mph to 60 mph for most of the study area with southbound speeds falling below 50 mph north of Thorne Lane in 2040. These slower speeds are attributed to the increase in traffic volumes through this area. The southbound AM peak hour Build alternative speeds are estimated to increase by nearly ten percent in 2020 and over 40 percent in 2040 as compared to the No Build Alternative. In the northbound direction the AM peak hour speeds increase by about 12 percent in both 2020 and 2040 as compared to the No Build Alternative speeds.

During the PM peak hour with the proposed improvements in 2020, northbound travel speeds along I-5 fall below 42 mph or LOS F (the shaded areas show speeds less than 42 mph ) north of the Berkeley Street Interchange as traffic volumes approach the practical capacity of the highway and drivers are changing lanes to enter and exit I-5. In the southbound direction in 2020, travel speeds along I-5 fall below 42 mph south of the Main Gate Interchange with speeds dropping to less than 10 mph , indicating area of stop-and-go traffic.

These slow speeds are caused by several factors, including the reduction of the number of southbound through travel lanes from four lanes to three lanes at Center Drive, the increase in traffic volumes, and drivers frequently change lanes to enter and exit l-5. However, these northbound speeds with the Build Alternative show a speed increase of more than 125 percent ( 44.2 mph vs. 19.4 mph ) as compared to the No Build Alternative in 2020. While the southbound Build Alternative average speeds are about the same as the No Build Alternative at 13 mph due primarily to the reduction in the number of through lanes.

During the PM peak hour with the proposed improvements in 2040, southbound PM peak hour travel speeds are generally less than 10 mph from Gravelly Lake Drive to Center Drive. These slow speeds reduce the number of vehicles that can travel through the corridor during the PM peak hour and prevent other cars from entering the corridor.

Figure 37: 2020 \& 2040 AM Peak Hour Travel Speed along I-5 from Center Drive to Gravelly Lake Drive - Build Alternative

## AM Peak Hour Travel Speeds along I-5-2020 Center Drive to Gravelly Lake Drive



AM Peak Hour Travel Speeds along I-5-2040 Center Drive to Gravelly Lake Drive

$\longrightarrow$ SB - 2040 Build
_-NB - 2040 Build

Based on the Meso Model data, estimates were made of the number of hours the travel speed operated below 70 percent of posted speed of 42 mph in 2020 and 2040. The analysis also showed that no hours of congestion are expected to occur during the AM peak period in 2020 and 2040, which correlates with the AM peak hour average travel speeds shown in Figure 36 above.

Figure 38: 2020 \& 2040 PM Peak Hour Travel Speed along l-5 from Center Drive to Gravelly Lake Drive - Build Alternative

PM Peak Hour Travel Speeds along I-5-2020 Center Drive to Gravelly Lake Drive


PM Peak Hour Travel Speeds along I-5-2040 Center Drive to Gravelly Lake Drive


During 2040 northbound PM peak hour, travel speeds on I-5 between Center Drive and Steilacoom-DuPont Road are generally above 50 mph because of the added travel lane at Center Drive. North of Steilacoom-DuPont Road, as traffic volumes increase and drivers frequently change lane to enter and exit I-5, travel speed fall below 42 mph . These slow average PM speeds signify severe congestion with slow moving vehicles and periods of stop-and-go traffic. In 2040, the southbound Build Alternative average travel speeds are less the No

Build Alternative speeds ( 7 mph vs 10 mph ); while the northbound Build Alternative average speeds increase by about 85 percent ( 27.3 mph for the Build alternative vs 14.8 mph for the No Build Alternative.) Southbound travel for the No Build Alternatives operates better south of Thorne Lane because the bottleneck occurs at the north end of the study area rather than at the south end, effectively metering the number of southbound vehicles using l-5 with the No Build Alternative. Figure 39 presents a summary map that illustrates and compares projected 2020 and 2040 travel speeds with the Build Alternative.

### 8.4 Peak Period I-5 Hours of Congestion - Build Alternative

During the PM peak period in 2020 and 2040, several hours of congestion are expected to occur along I-5 between Center Drive and Gravelly Lake Drive, as illustrated in Figure 40. During the 2020 PM peak period from two to four hours of congestion is expected northbound and southbound. During the 2040 PM peak period, congestion is expected to occur along the entire corridor in both directions that may last for nearly six hours.
These slow average speeds and hours of congestion expected during the PM peak period (2:00 PM and 8:00 PM) are also illustrated on the Congestion Contours shown in Figure 41. In 2020, southbound congestion would generally extend from north of the Main Gate Interchange to Center Drive. This congestion would be caused by the reduction in travel lanes from four lanes to three lanes at Center Drive and the high on-ramp volume at Center Drive. In the northbound direction in 2020, congestion would extend from around Berkeley Street to Bridgeport Way. In comparing these diagrams with the 2020 No Build Alternative diagrams, the duration and area of congestion is reduced.

By 2040, congestion is expected to extend past the 8:00 PM analysis period and would also extend north and south of the study area. In the southbound direction, congestion is expected to extend from Mounts Road past SR 512 for both the No Build and Build Alternatives. However, with the Build Alternative, there would generally be less congestion north of Berkeley Street. In the northbound direction during the 2040 PM peak period, congestion is expected to extend from north of Mounts Road with about one hour of congestion to nearly six hours of congestion at Bridgeport Way. South of Center Drive longer periods of congestion are expected.

Figure 39: 2020 and 2040 PM Peak Hour Travel Speeds on I-5 between Center Drive and Gravelly Lake Drive - Build Alternative


Figure 40: Hours of Congestion along I-5 during 2020 \& 2040 PM Peak Period from Center Drive to Gravelly Lake Drive - Build Alternative

PM Peak Period - Hours of Congestion along I-5-2020 Center Drive to Gravelly Lake Drive


PM Peak Period - Hours of Congestion along I-5-2040 Center Drive to Gravelly Lake Drive


Figure 41: Travel Speeds along I-5 during the 2020 \& 2040 PM Peak Period - Build Alternative

Southbound


Southbound


Northbound


Northbound


### 8.5 Peak Hour I-5 On and Off-Ramp Volumes - Build Alternative

On- and off-ramp volumes along l-5 between Center Drive and Gravelly Lake Drive would remain high in 2020 and 2040 peak hours for the Build Alternative. A comparison of the projected 2020 and 2040 AM peak hour on- and off-ramp volumes is shown in Figure 42. At these six interchanges there would be a total of about 3,840 vehicles exiting I-5 and 2,360 vehicles entering l-5 southbound in 2020, and about 3,660 vehicles exiting I-5 and 2,780 vehicles entering I-5 northbound in 2020 AM peak hour. The total of trips entering and exiting I-5 is more than the capacity of a single lane, and would require drivers to shift lanes.

Similarly, in 2040, there would be about 4,170 vehicles exiting l-5 and 2,750 vehicles entering $1-5$ at these six interchanges southbound, and about 3,900 vehicles exiting I-5 and 3,160 vehicles entering l-5 northbound. The total of trips entering and exiting l-5 would continue to be more than the capacity of a single lane, requiring drivers to shift lanes.

Figure 42: 2020 \& 2040 AM On- and Off-Ramp Volume along l-5 from Center Drive to Gravelly Lake Drive - Build Alternative

2020 AM Peak Hour On and Off-Ramp Volumes


2040 AM Peak Hour On and Off-Ramp Volumes


A comparison of the PM peak hour on- and off-ramp volumes in 2020 and 2040 is shown in Figure 43. Overall, at the interchanges along l-5 in the study area in 2020, there would be a total of about 2,210 vehicles exiting I-5 and 4,150 vehicles entering I-5 southbound, and about 2,800 vehicles exiting $1-5$ and 5,160 vehicles entering $1-5$ northbound.

Similarly, in 2040, there would be about 1,590 vehicles exiting l-5 and 4,430 vehicles entering I5 at these interchanges southbound, and about 2,600 vehicles exiting $1-5$ and 4,820 vehicles entering l-5 at the study area interchanges northbound.

As with the existing conditions and the No Build Alternative, all of this traffic cannot be in the outside lane at the same time, so drivers must frequently change lanes to enter and exit I-5. This heavy amount of lane change movement would cause traffic to slow, increase congestion, and reduce the overall traffic throughput in the JBLM area.

Figure 43: 2020 \& 2040 PM On- and Off-Ramp Volume along I-5 from Center Drive to Gravelly Lake Drive - Build Alternative

2020 PM Peak Hour On and Off-Ramp Volumes


2040 PM Peak Hour On and Off-Ramp Volumes


As compared to the 2020 and 2040 No Build Alternative on- and off-ramp volumes, these 2020 and 2040 Build Alternative ramp volumes would generally be within plus or minus 10 percent.

### 8.6 Comparison of I-5 Travel Times - No Build Alternative vs Build Alternative

A comparison of No Build Alternative travel times along I-5 between Center Drive and Gravelly Lake Drive was made using output from the Meso Model and is shown in Figure 44 for the AM and PM peak hours. Traveling along I-5 between Center Drive and Gravelly Lake Drive at the
posted speed limit would normally take about 8.2 minutes to cover the 8.2 miles between the two interchanges.

Figure 44: 2020 Cumulative PM Peak Hour Travel Times along I-5 between Center Drive and Gravelly Lake Drive -2020 No Build Alternative and Build Alternative


I-5 Southbound Cumulative Travel Time-2020 PM Peak Hour
Gravelly Lake Drive to Center Drive


Comparisons of No Build Alternative and Build Alternative travel times along l-5 between Center Drive and Gravelly Lake Drive were made using output from the Mesoscopic Model and
are shown in Figures 45 and 46 for 2020 and 2040 AM and PM peak hours, respectively. Traveling along l-5 between Center Drive and Gravelly Lake Drive at the posted speed limit would require about 8.2 minutes to cover the 8.2 miles between the two interchanges.

As shown on Figure 45, I-5 northbound and southbound travel times during the AM 2020 peak hour between these interchanges would be about the same for the No Build and the Build Alternatives as 2013 conditions (i.e. around eight to nine minutes). Traffic during the time would generally operate near the posted speed limit.

During the 2020 PM peak period, overall southbound travel along l-5 between Center Drive and Gravelly Lake Drive with either the No Build or Build Alternatives would take about 37 to 39 minutes. However, along I-5 north of the Main Gate Interchange, the Build Alternative would show better travel times than the 2013 conditions, and up to 25 minutes shorter travel times than the No Build Alternative. South of the Main Gate Interchange, where Build Alternative speeds are reduced because of the reduction in travel lanes from four lanes to three lanes at Center Drive, travel time are expected to increase relative to the No Build Alternative.

During the 2020 PM peak period, northbound travel along l-5 from Center Drive to Gravelly Lake Drive for the Build Alternative would be slightly better than the 2013 conditions (11 minutes vs 12 minutes) and about 15 minutes shorter compared to the 2020 No Build Alternative ( 11 minutes vs 26 minutes).

Figure 46 shows the 2040 AM and PM cumulative peak hour travel times along I-5 between Center Drive and Gravelly Lake Drive. During the AM peak hour, travel times with the Build Alternative would be similar to the 2013 conditions with overall travel times between Center Drive and Gravelly Lake Drive between eight and nine minutes. The 2040 No Build Alternative travel times would be about 12 minutes southbound and nine minutes northbound.

During the 2040 PM peak hour, northbound travel times on I-5 with the Build Alternative are expected to be similar to 2013 conditions from Center Drive to Berkeley Street, and then slightly increase such that overall travel time is about 12 minutes in 2013 and would be 18 minutes in 2040. The increase in northbound travel time would be caused by maintaining four lanes through the corridor with the Build Alternative, which allows more volume and results in slower traffic speeds. In 2013, only three lanes are available south of Thorne Lane and the increase to four lane allows northbound traffic to operate at slightly higher speeds. In contrast, travel time with the No Build Alternative is expected to increase to about 34 minutes because of the higher demand with the same number of lanes as with 2013 conditions.

Figure 45: Comparison of No Build vs Build Alternatives for 2020 AM \& PM Peak Hour Cumulative Travel Times through the Study Area


Figure 46: Comparison of No Build vs Build Alternatives for 2040 AM \& PM Peak Hour Cumulative Travel Times through the Study Area


Conversely in the southbound direction, 2040 PM peak hour travel times with the Build Alternative are expected to be higher than the No Build Alternative ( 68 minutes vs 48 minutes). For the Build Alternative, the southbound four-lane to three-lane reduction is moved from Thorne Lane to Center Drive. For the 2040 No Build Alternative, congestion extends southward to around the Main Gate Interchange with some congestion at the Center Drive on-ramp. Because of the lower amount of traffic flowing through the corridor, No Build Alternative travel speeds are slightly higher along the corridor. With the Build Alternative, the reduction in travel lanes at Center Drive would allow more traffic on I-5 but travel speeds would be slower and back-ups would extend throughout the corridor which increases travel times.

### 8.7 Summary of Future Year Intersection Analysis at l-5 Reconfigured and Adjacent Interchanges for the Build Alternative

The Build Alternative intersection analyses were conducted using Synchro software for signalized and non-signalized intersections and Sidra software for roundabouts for a 2020 opening year and a 2040 design year. Results of the analyses for the two focus interchanges are summarized in Table 6. The analyses show that during the AM and PM peak hours with the revised interchange configurations with roundabouts for the Build Alternative, intersections at the Berkeley Street Interchange and Thorne Lane Interchange all operate at LOS C or better and operate better than the No Build Alternative. A comparison between 2020 AM and PM peak hour LOS results for the No Build and Build Alternatives is presented graphically in Figures 47 and 48.

The intersection analyses for the Berkeley Street, Thorne

| INTERSECTION LEVEL OF SERVICE <br> (LOS) CRITERIA |  |  |
| :---: | :---: | :---: |
|  | Signalized <br> Intersection | Unsignalized <br> Intersection |
| LOS | Delay (sec) | Delay (sec) |
| A | $\leq 10$ sec | $\leq 10$ sec |
| B | $10-20$ sec | $10-15$ sec |
| C | $20-35$ sec | $15-25$ sec |
| D | $35-55$ sec | $25-35$ sec |
| E | $55-80$ sec | $35-50$ sec |
| F | $\geq 80$ sec | $\geq 50$ sec |
| Source: 2010 Highway Capacity |  |  | Lane and Gravelly Lake Drive intersections used Synchro software for signalized and nonsignalized intersections and Sidra software for roundabouts. Turning movement volumes at each intersection were developed through the use of the Meso Model.

Berkeley Street Interchange - In addition to providing grade separation over the adjacent rail line, the proposed Build Alternative reconfiguration for the Berkeley Street interchange with teardrop roundabouts would improve traffic operations at this interchange. Overall, the levels of service at the Berkeley Street intersections are expected to be LOS C or better for the Build Alternative, and the teardrop roundabouts would operate at LOS B or better. For the No Build Alternative, the levels of service at the Berkeley Street intersections with the I-5 ramp would be LOS D or better with the interim Madigan Access improvements.

Table 6: Summary of Interchange Delay and Level of Service (LOS) at the Reconfigured Interchanges-No Build vs. Build Alternative

| Intersection* | 2020 No Build |  | 2020 Build |  | 2040 No Build |  | 2040 Build |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | AM | PM | AM | PM | AM | PM | AM | PM |
| I-5 NB Ramps / Berkeley Street |  |  |  |  |  |  |  |  |
| Control Type | Signal** |  | Roundabout |  | Signal** |  | Roundabout |  |
| Average Delay (sec) / LOS | 16.3/B | 20.8/C | 4.4/A | 5.2/A | 11.4/B | 14.5/B | 4.5/A | 4.6/A |
| l-5 SB Ramps / Berkeley Street |  |  |  |  |  |  |  |  |
| Control Type | Signal** |  | Roundabout |  | Signal** |  | Roundabout |  |
| Average Delay (sec) / LOS | 36.0/D | 26.0/C | 13.2/B | 9.1/A | 32.4/C | 23.8/C | 16.7/B | 8.7/A |
| Berkeley Street / Union Avenue** |  |  |  |  |  |  |  |  |
| Control Type | Signal |  | 2-Way Stop |  | Signal |  | 2-Way Stop |  |
| Average Delay (sec) / LOS | 11.0/B | 12.0/B | 15.2/C | 9.0/A | 10.0/B | 12.7/B | 15.5/C | 13.2/B |
| Berkeley Street / Washington Avenue |  |  |  |  |  |  |  |  |
| Control Type | 2-Way Stop |  | 2-Way Stop |  | 2-Way Stop |  | 2-Way Stop |  |
| Average Delay (sec) / LOS | 12.6/B | 14.3/B | 9.3/A | 9.2/A | 14.2/B | 12.2/B | 9.6/A | 9.2/B |
| Berkeley Street / Jackson Avenue Extension |  |  |  |  |  |  |  |  |
| Control Type | NA |  | All-way Stop |  | NA |  | All-way Stop |  |
| Average Delay (sec) / LOS | NA | NA | 13.9/B | 23.8/C | NA | NA | 12.3/B | 10.9/B |

l-5 NB Ramps / Thorne Lane

| Control Type | Signal |  | Roundabout |  | Signal |  | Roundabout |  |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Average Delay (sec) / LOS | 34.2/C | $37.9 / \mathrm{D}$ | $5.5 / \mathrm{A}$ | $7.1 / \mathrm{A}$ | $37.3 / \mathrm{D}$ | $36.6 / \mathrm{D}$ | $7.0 / \mathrm{A}$ | $11.9 / \mathrm{B}$ |

I-5 SB Ramps / Thorne Lane

| Control Type | Signal |  | Roundabout |  | Signal |  | Roundabout |  |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Average Delay (sec) / LOS | $33.9 / \mathrm{C}$ | $47.5 / \mathrm{D}$ | $8.8 / \mathrm{A}$ | $14.6 / \mathrm{B}$ | $49.5 / \mathrm{D}$ | $44.4 / \mathrm{D}$ | $12.6 / \mathrm{B}$ | $17.7 / \mathrm{B}$ |

Thorne Lane/Union Avenue Loop (New Intersection)

| Control Type | NA |  | Roundabout |  | NA |  | Roundabout |  |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Average Delay (sec) / LOS | NA | NA | $6.5 / \mathrm{A}$ | $21.1 / \mathrm{C}$ | NA | NA | 6.9/A | $9.1 / \mathrm{A}$ |


| Thorne Lane / Union Avenue (with Gravelly-Thorne Connector for Build Alternative) |
| :--- |
| Control Type <br>  <br> Average Delay (sec) / LOS 2-way Stop |

Notes* Signalized \& non-signalized intersections analyzed using Synchro software and Highway Capacity Manual procedures. Please note that the Synchro analysis does not account for back-ups on on-ramp from the ramp meter or freeway.
** Assumes Madigan Access Improvements at the Berkeley Street Interchange are implemented with the No Build Alternative by 2020.

Thorne Lane Interchange - The proposed Build Alternative reconfiguration with teardrop roundabouts at the l-5 ramps and grade separation over the adjacent rail line would improve traffic operations at this interchange. At the Thorne Lane intersections with the I-5 ramps, the levels of service for the No Build Alternative would generally be at LOS D or better. The reconfigured Build Alternative interchange is expected to operate at LOS B or better through 2040. Results of the intersection analyses for the adjacent interchanges at Center Drive, Steilacoom-DuPont Road and Gravelly Lake Drive are summarized in Table 7.

Figure 47: 2020 AM and PM Peak Hour Levels of Service for the No Build and Build Alternatives
PEAK HOUR LEVELS OF SERVICE - 2020


Figure 48: 2040 AM and PM Peak Hour Levels of Service for the No Build and Build Alternatives

## PEAK HOUR LEVELS OF SERVICE - 2040



Table 7: Summary of Interchange Delay and Level of Service (LOS) at Other Area Interchanges-No Build vs. Build Alternatives

| Intersection* | 2020 No Build |  | 2020 Build |  | 2040 No Build |  | 2040 Build |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | AM | PM | AM | PM | AM | PM | AM | PM |
| I-5 NB Ramps / Center Drive** |  |  |  |  |  |  |  |  |
| Control Type | 2-way Stop |  | 2-way Stop |  | 2-way Stop |  | 2-way Stop |  |
| Average Delay (sec) / LOS | 12.3/B | 12.7/B | 12.2/B | 10.9/B | 12.0/B | 11.9/B | 13.3/B | 15.0/C |
| l-5 SB Ramps / Center Driv |  |  |  |  |  |  |  |  |
| Control Type | 2-way Stop |  | 2-way Stop |  | 2-way Stop |  | 2-way Stop |  |
| Average Delay (sec) / LOS | 18.6/C | 13.3/B | 15.3/C | 11.4/B | 35.0/E | 13.2/B | 21.0/C | 63.1/F |


| Center Drive / Wilmington Drive |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Control Type <br> Average Delay (sec) / LOS | Signal |  | Signal |  | Signal |  | Signal |  |
|  | 14.1/B | 20.2/C | 13.0/B | 18.6/B | 18.4/B | 20.2/C | 13.7/B | 18.7/B |


| I-5 NB Ramps / Steilacoom-DuPont Road |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Control Type <br> Average Delay (sec) / LOS | Signal |  | Signal |  | Signal |  | Signal |  |
|  | 22.5/C | 45.1/D | 22.3/C | 43.8/D | 29.7/C | 57.9/E | 28.6/C | 49.3/D |
| l-5 SB Ramps / Steilacoom-DuPont Road |  |  |  |  |  |  |  |  |
| Control Type | Signal |  | Signal |  | Signal |  | Signal |  |
| Average Delay (sec) / LOS | 34.0/C | 29.1/C | 37.2/D | 41.2/D | 68.7/E | 37.5/D | 82.2/F | 30.9/C |
| Steilacoom-DuPont Road / Barksdale Avenue / Wilmington Drive |  |  |  |  |  |  |  |  |
| Control Type | Signal |  | Signal |  | Signal |  | Signal |  |
| Average Delay (sec) / LOS | 36.9/D | 27.1/C | 46.9/D | 37.4/D | 58.2/E | 26.6/C | 50.3/D | 28.5/ |

I-5 NB Ramps / Gravelly Lake Drive

| Control Type | Signal |  | Signal |  | Signal |  | Signal |  |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :---: |
| Average Delay (sec)/LOS | $46.5 / \mathrm{D}$ | $46.1 / \mathrm{D}$ | $24.0 / \mathrm{C}$ | 35.0/C | 35.4/D | $49.6 / \mathrm{D}$ | $26.1 / \mathrm{C}$ |  |
| 50.2/D |  |  |  |  |  |  |  |  |

I-5 SB Ramps / Gravelly Lake Drive

| Control Type | Signal |  | Signal |  | Signal |  | Signal |  |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Average Delay (sec)/LOS | 31.3/C | 37.2/D | 38.4/D | 37.9/D | 32.8/C | 40.8/D | 47.0/D | 39.3/D |

## Gravelly Lake Drive / Pacific Highway

| Control Type | Signal |  | Signal |  | Signal |  | Signal |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Average Delay (sec) / LOS | 32.0/C | 37.1/D | 12.6/B | 17.9/B | 34.6/C | 34.7/C | 15.8/B | 12.8/B |

Notes: * Signalized \& non-signalized intersections analyzed using Synchro software and Highway Capacity Manual procedures Please note that the Synchro analysis does not account for back-ups on on-ramp from the ramp meter or freeway.
** The I-5 NB Ramps / Center Drive intersection was redesigned in 2015. This new design is reflected in the 2020 and 2040 analysis.

Center Drive - For the northbound and southbound ramp intersections at Center Drive for the Build Alternative, the Synchro analyses show that these intersections would operate at LOS C or better in 2020 and 2040 during the AM and PM peak hours, except that the I-5 southbound ramp intersection for the Build Alternative is expected to operate at LOS E in the PM Peak hour. However, the Synchro analysis does not account for back-ups from the ramp meter on the southbound on-ramp.

For both the No Build and Build Alternatives, traffic at the Center Drive southbound on-ramp is expected to back-up from the ramp meter through the l-5 southbound ramp intersection with Center Drive and then westbound along Center Drive and through the signalized intersections at Wilmington Drive and McNeil Street. Figure 49 shows the 2020 PM peak hour queue backups along Center Drive from the l-5 southbound ramp intersection with Center Drive and along Wilmington Drive west of Center Drive.

With the Build Alternative, queues along Center Drive would increase by about 1,050 feet, and along Wilmington Drive by about 325 feet. The increases in traffic queues along Center Drive and Wilmington Drive with the Build Alternative would be partially due to traffic re-routing in the area caused mainline congestion north of Center Drive, and the reduction of I-5 travel lanes at Center Drive from four lanes to three lanes.

To provide a quantitative assessment of expected future traffic operations at this location that does account for the effects of traffic queuing, further analysis was conducted using the Meso Model (Dynameq). Results are presented in Table 8.

Steilacoom-DuPont Road - For the No Build Alternative, the level of service at the northbound Steilacoom-DuPont Road intersection with the l-5 ramps is expected to be LOS D during the AM peak hour, but dropping to LOS F during the PM peak hour. LOS C is expected at the southbound ramp intersection during the AM peak hour, dropping to LOS D during the PM peak hour. For the Steilacoom-DuPont Road intersection with Barksdale Avenue and Wilmington Drive, the level of service is expected to be LOS C during the AM peak hour, dropping to LOS F during the PM peak hour.

With the Build Alternative, the northbound ramp intersection is expected to operate at LOS C during the AM peak hour and LOS E during the PM peak hour. Operations would improve to LOS C or better at the southbound ramp intersection during both the AM and PM peak hours. At Barksdale Avenue and Wilmington Drive, the AM peak hour is expected to operate at LOS C, dropping to LOS E during the PM peak hour.

Gravelly Lake Drive - During the 2020 AM and PM peak hours, the ramp intersections at Gravelly Lake Drive are expected to operate at LOS D or better for both the No Build and Build Alternatives. At the intersection of Gravelly Lake Drive and Pacific Highway, the PM peak hour LOS would be D or better for the No Build Alternative, but is expected to improve to LOS $B$ with the Build Alternative.

A more detailed summary of the intersection analyses for the Build Alternative, including turning movements for both the Synchro analyses and from the Mesoscopic Model, is contained in Appendix F.

Figure 49: Comparison of No Build vs. Build Alternatives 2020 PM Peak Hour of 95 \% Traffic Queues along Center Drive and Wilmington Drive in DuPont


Table 8: 2020 AM and PM Peak Hour Intersection Level of Service at Center Drive Interchange using Meso Model - No Build and Build Alternatives

| Intersection * | 2020 No Build |  | 2020 Build |  |
| :---: | :---: | :---: | :---: | :---: |
|  | AM | PM | AM | PM |
| I-5 NB Ramps/Center Drive** (2-Way Stop ) |  |  |  |  |
| Average Delay (sec) / LOS | 8/A | 4/A | 2/A | 5/A |
| I-5 SB Ramps/Center Drive (2-Way Stop) |  |  |  |  |
| Average Delay (sec) / LOS | 10/B | 66/F | 2/A | 61/E |
| Center Drive/Wilmington Drive(Signal) |  |  |  |  |
| Average Delay (sec) / LOS | 9/A | 59/E | 9/A | 75/E |

[^1]Main Gate/41st Division Drive Interchange - As the I-5 / Main Gate interchange ramp terminals have no signalized or stop-controlled intersections, a separate analysis was conducted for the cloverleaf design at this interchange, focusing on the ramp connections to 41st Division Drive. Analysis was conducted using output from the Meso Model, as shown in Table 9. The analysis shows that the northbound approach along 41st Division Drive would have long delays (nearly five minutes) at the northbound ramp connections for the No Build Alternative in the PM peak hour, while there would be minimal delay on the other approaches. At the southbound ramp connections, delays would be less than 30 seconds on all approaches.

For the Build Alternative, traffic operations are expected to improve with delays of less than 37 seconds for all approaches at the northbound ramp connections to 41st Division Drive. The southbound ramp connections would have slightly lower delays of approximately 25 seconds or less for all approaches along 41st Division Drive. Overall, the Main Gate interchange is expected to perform better and to experience lower average delays than with the No Build Alternative.

Table 9: 2020 Delay Summary at Main Gate Interchange - No Build vs. Build Alternative

| Approach | 2020 No Build |  | 2020 Build |  |
| :---: | :---: | :---: | :---: | :---: |
|  | Volume AM/PM | Delay (seconds per vehicle) AM/PM | Volume AM/PM | Delay (seconds per vehicle) AM/PM |
| NB I-5 Ramp / 41 ${ }^{\text {st }}$ Division Drive |  |  |  |  |
| NB on $41^{\text {st }}$ Division Drive | 710/1,835 | 4.7/294 | 735/1,395 | 4.0/36.4 |
| SB on 41 ${ }^{\text {st }}$ Division Drive | 1,220/1,075 | 0.3/1.6 | 1,220/995 | 0.4/13.8 |
| EB on l-5 NB Off-ramp | 305/50 | 0.0/0.0 | 300/80 | 0.0/0.0 |
| WB on l-5 NB Loop Off-ramp | 75/25 | 0.0/0.0 | 65/40 | 0.0/0.0 |
| SB I-5 Ramp / 41st Division Drive |  |  |  |  |
| NB on 41st Division Drive | 525/1,425 | 0.3/0.9 | 530/915 | 0.4/24.6 |
| SB on 41st Division Drive | 1,015/1,435 | 2.5/28.2 | 1,060/990 | 2.1/3.2 |
| EB on I-5 NB Loop Off-ramp | 390/50 | 0.8/0.7 | 345/125 | 0.7/0.3 |
| WB on l-5 NB Off-ramp | 120/50 | 0.5/0.0 | 135/165 | 0.5/9.9 |

### 8.8 Summary of 2020 and 2040 I-5 Traffic Conditions in the JBLM vicinity

A summary of the key findings from the l-5 traffic operation analysis of the No Build Alternative and the Build Alternative in 2020 and 2040 include:

- Traffic demand along I-5 in the JBLM area remains high but the Build Alternative accommodates a higher percent of trip demand during the PM peak hours than the No

Build Alternative ( 92.6 percent vs 71.4 percent in 2020 and 49.0 percent vs 30.4 percent in 2040).

- 2020 PM northbound I-5 travel speeds average 44 mph with the Build Alternative and 19 mph with the No Build Alternative.
- 2020 PM southbound I-5 travel speeds average about 13 mph for both the Build and No Build Alternatives.
- 2040 PM northbound I-5 travel speeds average 27 mph with the Build Alternative and 15 mph with the No Build Alternative.
- 2040 PM southbound I-5 travel speeds average about 7 mph for the Build Alternative and about 10 mph for the No Build Alternative. The slightly lower Build Alternative average speed is caused by moving the reduction in travel lanes from Thorne Lane for the No Build Alternative to Center Drive for the Build Alternative. This change causes slower southbound traffic through most of the study area, whereas the No Build Alternative causes more back-up outside the study area.
- The No Build Alternative has congestion lasting for up to 4.5 hours through most of the study area, whereas the Build Alternative has congestion lasting between two and four hours during the six-hour PM peak analysis period.
- High levels of exiting and entering traffic from several ramps cause drivers to shift lanes frequently, resulting in slow travel speeds for both the No Build Alternative and the Build Alternative.
- Average AM travel times in 2020 along the I-5 corridor between Center Drive and Gravelly Lake Drive are lower in both directions with the Build Alternative as compared to the No Build Alternative.
- Average PM travel times in 2040 along the l-5 corridor between Center Drive and Gravelly Lake Drive are lower in the northbound direction with the Build Alternative as compared to the No Build Alternative. However, in the PM southbound direction average travel times are higher for the Build Alternative, because of the higher demand, moving the lane reduction to Center Drive, and the high merging traffic from Center Drive.
- With the interchange improvements at Steilacoom-DuPont Road, Berkeley Street and Thorne Lane, intersection operations are at LOS C or better in both 2020 and 2040 for the Build Alternative; whereas several ramp intersections are at LOS E or F with the No Build Alternative.


### 9.0 I-5 Collision Analysis

A five-year collision analysis was conducted along the I-5 mainline from milepost (MP) 117.42 (south of the Center Drive Interchange) to MP 124.79 (north of the Gravelly Lake Drive Interchange) using data from January 2010 through December 2014. This analysis of mainline, ramp and cross street collisions within the limited access area included a review of the existing collision rate, location,
"Under Section 409 of Title 23 of the United States Code, any collision data furnished is prohibited from use in any litigation against state, tribe or local government that involves the location(s) mentioned in the collision data." severity, type, and contributing factors.

During this five-year period there were 1,963 reported collisions along the l-5 corridor, an average of more than one collision per day. Approximately 84 percent occurred on the l-5 mainline with 16 percent occurring at the six interchanges between Center Drive and Gravelly Lake Drive and in the limited-access segments of the cross streets, as indicated by Figure 50.

### 9.1 Collision Rates

A summary of the annual collision rates by severity of collisions along the l-5 mainline is shown in Table 10. Table 10 shows the total collisions along the mainline, ramps and all cross-streets within the limited access area.

Table 10: Collision Summary on I-5 from Center Drive to Gravelly Lake Drive
$\left.\left.\begin{array}{lccc}\hline \begin{array}{l}\text { Severity of Collisions } \\ \text { Mainline, Ramps and } \\ \text { Cross Streets }\end{array} & \mathbf{2 0 1 0} \text { to 2014 Collisions }\end{array} \quad \begin{array}{c}\text { Average Annual } \\ \text { Collisions }\end{array}\right) ~ \begin{array}{c}\text { Collision Rate per 100 } \\ \text { MVMT * }\end{array}\right\}$
*100 MVMT = 100 Million Vehicle Miles Traveled
The average collision rates on I-5 through the JBLM area, based on available data, are below the Pierce County collision rate for all highways ( 177.5 collisions per 100 MVMT), as documented in WSDOT's 2013 Annual Collision Summary. Fatalities and serious injury rates are also below the county wide averages of 0.62 fatalities per 100 MVMT and 3.36 serious injuries per 100 MVMT.

WSDOT has also conducted a safety assessment for all state highways in Washington State. Based on WSDOT's 2015 safety assessment, using 2009-2013 data, WSDOT identified four Collision Analysis Segments (CAS) located on I-5 within the study area, as shown in Table 11. One is in the vicinity of Center Drive, two are near Steilacoom-DuPont Road and one is from Thorne Lane to Bridgeport Way. The recently completed Tiger III improvements can improve these locations, but two years of data are needed to assess the effectiveness of the ramp meters and other improvements.

Table 11: Location of IU-5 Mainline, Ramp and Cross Street Collision Summary

| Highway | From Location | To Location |
| :---: | :---: | :---: |
| I-5 | NB off-ramp to Center Drive Gore | 0.18 miles north of Center Drive bridge |
|  | MP 117.79 | MP 118.14 |
| I-5 | Bridge over Railroad to JBLM | Mt SB on-ramp from Steilacoom-DuPont Road |
|  | MP 118.37 | MP 118.64 |
| I-5 | At SB on-ramp from Steilacoom-DuPont Road | Bridge over Pendleton Avenue |
|  | MP 118.64 | MP 119.38 |
| I-5 | SB Off-ramp to Thorne Lane | Bridge over Clover Creek near Bridgeport Way |
| MP 123.94 |  | MP 125.64 |

### 9.2 I-5 Mainline Collision

The locations of collisions along the l-5 mainline and the time of day they occur over the fiveyear period from 2010 through 2014 are discussed below.

Location of I-5 Collisions: With 84 percent ( 1,635 collisions of five years) of the collisions between Center Drive and Gravelly Lake Drive occur along the l-5 mainline, an analysis was conducted to determine the location of collisions. Figure 51 shows the location and number of collisions along the l-5 corridor by milepost in both directions over the five-year period from January 2010 through December 2014. With the close proximity of interchanges and heavy merging and existing volumes, many of the collisions occur near the interchange on- and offramps, or as drivers merge across traffic to change lanes. At the Thorne Lane Interchange, southbound collisions are high because of the outside lane becoming an exit only lane and through traffic in this lane must change lanes to continue south.

Collisions by Time of Day: Figure 52 shows the distribution of mainline collision by time of day over the five year (2010 to 2014) period along l-5 between Center Drive and Gravelly Lake Drive. Approximately 14 percent of the collision along I-5 occur between 5:00 AM and 7:00 AM, and over 48 percent of the collisions occur between 3:00 PM and 7:00 PM. These times of collision generally correspond AM and PM peak travel times with the most congestion

Figure 51: I-5 Mainline Collisions by Milepost


Note: Under Section 409 of Title 23 of the United States Code, any collision data furnished is prohibited from use in any litigation against state, tribe or local government that involves the location(s) mentioned in the collision data."

Figure 52: Distribution of I-5 Collisions by Time of Day between Center Drive and Gravelly Lake Drive
Distribution of l-5 Collisions by Time of Day from Mounts Road to Gravelly Lake Drive -- 2010 to 2014


Note: Under Section 409 of Title 23 of the United States Code, any collision data furnished is prohibited from use in any litigation against state, tribe or local government that involves the location(s) mentioned in the collision data."

### 9.3 Severity, Type and Contributing Circumstance for I-5 Collisions

An analysis of all l-5 collisions, including mainline, ramp and cross street collisions, between Center Drive and Gravelly Lake Drive was conducted to determine the severity, types, and contributing circumstances of the collisions.

Severity of I-5 Collisions: The severity of the $\mathrm{I}-5$ collisions is summarized in Figure 53. Collisions involving property damage only (no injuries) make up the majority (nearly 72 percent) of the collisions with almost 83 percent of these collisions occurring along the I-5 corridor between Center Drive and Gravelly Lake Drive. Three fatalities occurred along l-5 during the five-year study period and 19 collisions involved serious injuries.

Types of I-5 Collisions: As shown in Figure 54, nearly 70 percent of collisions along the I5 corridor between Center Drive and Gravelly Lake Drive were rear-end collisions and almost 20 percent were sideswipe collisions. About seven percent of the collisions involve hitting fixed objects, such as median barriers, guardrails, retaining walls, fences, bridges, and ditches. The rear-end and sideswipe collisions are common occurrences in congested stop-and-go conditions, like l-5 through the study area with heavy entering and exiting traffic and drivers frequently changing lanes.

Figure 53: Severity of I-5 Collisions - Center Drive to Gravelly Lake Drive - 2010 to 2014


Figure 54: l-5 Collisions by Type - Center Drive to Gravelly Lake Drive - 2010 to 2014


Contributing Circumstances for I-5 Collisions: Based on existing collision data, there are several circumstances that contribute to the collisions along the l-5 corridor between Center Drive and Gravelly Lake Drive, as shown on Figure 55. Exceeding reasonable speeds, following too closely, and driver inattention are three factors that contribute to 71 percent of the collisions that have occurred along this

Figure 55: Contributing Circumstances for I-5 Collisions - Center Drive to Gravelly Lake Drive - 2010 to 2014
 section of I-5. Drivers who were distracted or did not grant others the right of way to merge or change lanes contributed another 12 percent of the collisions along the l-5.

### 9.4 Effect of Collision on the Traffic Flow and Speeds along I-5

Figure 56 illustrates the effect of a collision on traffic congestion along l-5 through the study area. Data were obtained for a specific incident that occurred at approximately 2 PM on February 28, 2013 in the southbound directions of I-5. Traffic did not clear and begin to move until 4 PM. Northbound traffic remained slow until 7 PM and southbound traffic did not resume normal speeds until after 8 PM.

Figure 56: Speeds on I-5 between Exits 114 and 127 with a 2 PM Crash


### 9.5 Effect of Proposed Build Alternative on I-5 Collisions

The Build Alternative is expected to improve operations in the opening year of operation, add capacity, reduce congestion, and reduce mainline collisions. In addition, the reconfigured interchanges with roundabouts and longer ramps at Berkeley Street and Thorne Lane are expected to reduce collisions at the ramp terminals by reducing the number of conflict points as compared to signalized intersections. Also, the ramps are designed with longer queue areas that would reduce queue backing up onto the I-5 mainline, resulting in less traffic flow interruptions along l-5 and reduced collisions. By the 2040 design year, congestion would once again become a dominant pattern and other improvements would be needed to reduce collisions.

To quantitatively assess the expected effect of the Build Alternative on safety a future year collision analysis was conducted using the Enhanced Interchange Safety Analysis Tool (ISATe) developed for the National Cooperative Highway Research Program. This model estimates future year collisions based on projected traffic volumes and the geometric design of the proposed interstate and interchanges for the No Build and Build Alternatives. A summary of the ISATe model results is located in Appendix G.

For the No Build Alternative, with future year traffic demand and increased congestion without any major capacity improvements, the number of collisions along l-5 is expected to increase between 2013 and 2020 and beyond to 2040. For the Build Alternative with improved interchanges and added capacity, collisions along I-5 and at the interchanges in 2020 and 2040 are expected to be higher than the No Build Alternative because of higher expected traffic levels along the l-5 corridor, as shown in Table 12. However, the overall collision rate per million vehicles is slightly lower for the Build Alternative than for the No Build Alternative.

Table 12: Comparison of 2020 and 2040 Predicted Collisions on I-5 - Center Drive Interchange to Gravelly Lake Drive Interchange

|  |  |  | Ramp Intersection |  |  |  |  |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Mainline Collisions | Ramp Collisions | Collisions |  |  |  |  |

Notes:
MVM = Million vehicle miles
MEV = Million entering vehicles
Based on average traffic volumes at the permanent count location south of the Main Gate Interchange

### 10.0 Effects of the Build Alternative on Local Streets and Intersections

The redesign and relocation of the interchanges at Thorne Lane and Berkeley Street would affect local travel patterns and change how drivers access l-5 from the local street system. Traffic on local roads would also be affected by the amount of congestion on I-5. As congestion increases on I-5, either northbound or southbound, more traffic is expected to shift to local roads. In addition, some drivers may use alternate interchanges to reach their final destination, depending on the level of congestion on I-5. Traffic changes caused by the reconfiguration of the Thorne Lane and Berkeley Street interchanges, the addition of I-5 travel and auxiliary lanes, and the Gravelly-Thorne Connector are discussed below.

Thorne Lane: At Thorne Lane, the existing bridge over I-5 is proposed to be removed and replaced with a new bridge about 350 feet to the south that would grade-separate Thorne Lane over I-5, the adjacent rail line and Union Avenue, as previously shown in Figure 30. The new bridge would change part of the Thorne Lane and Murray Road alignment to connect to the existing street system. In addition, a new loop connector road would be added to tie Union Avenue to Thorne Lane. The proposed southbound Gravelly-Thorne Connector and the new northbound auxiliary lane between the Thorne Lane and Gravelly lake Drive interchanges would also affect traffic movements to and from the Tillicum and Woodbrook neighborhoods. The new interchange is proposed to have roundabouts at the I-5 ramp intersections instead of traffic signals.

These interchange revisions, together with the new southbound only Gravelly-Thorne Connector roadway and northbound auxiliary lane between Thorne Lane and Gravelly Lake Drive, would likely affect local travel patterns in the vicinity of the Thorne Lane interchange. Because of the Gravelly-Thorne Connector, some trips would be diverted from I-5 and would use the new roadway connected to Union Avenue near Thorne Lane. This diversion is an intended benefit of the proposed Build Alternative.

Changes in two-way traffic volumes on local roads near the Thorne Lane interchange are shown in Table 13 for the No Build and Build Alternatives. With the No Build Alternative, two-way traffic along Union Avenue near Thorne Lane in 2020 and 2040 is expected to be approximately 355 vehicles during the AM peak hour, and around 525 vehicles during the PM peak hour. With the Build Alternative, AM peak hour two-way volume on Union Avenue is expected to be less than 205 vehicles in 2020 and 2040, and the PM peak hour volume would be about 290 vehicles in 2020, but reduced to about 185 vehicles by 2040. In general, volumes on Union Avenue are expected to be lower with the Build Alternative as a result of the added capacity on I-5 and the improved interchanges.

Table 13: 2020 and 2040 AM and PM Peak Hour Two-way Volumes on Local Streets near the Thorne Lane Interchange - No Build Alternative vs. Build Alternative

|  | No Build Alternative |  |  |  | Build Alternative |  |  |  |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Location | $\mathbf{2 0 2 0}$ | $\mathbf{2 0 2 0}$ | $\mathbf{2 0 4 0}$ | $\mathbf{2 0 4 0}$ | $\mathbf{2 0 2 0}$ | $\mathbf{2 0 2 0}$ | $\mathbf{2 0 4 0}$ | $\mathbf{2 0 4 0}$ |
| AM | PM | AM | PM | AM | PM | AM | PM |  |
| Union Avenue south of Thorne Lane | 355 | 525 | 390 | 385 | 205 | $\mathbf{2 9 0}$ | 180 | 185 |
| Thorne Lane west of Union Avenue or |  |  |  |  |  |  |  |  |
| Union Avenue Loop Connector | 375 | 570 | 440 | 455 | 590 | 1,180 | 705 | 885 |
| Thorne Lane over I-5 |  |  |  |  |  |  |  |  |

On Thorne Lane west of Union Avenue, compared to the No Build Alternative traffic is expected to increase with the Build Alternative during the AM peak hour by about 215 vehicles in 2020 and by about 265 vehicles in 2040. It is expected to increase during the PM peak hour by about 610 vehicles in 2020 and by about 430 vehicles in 2040 . On the bridge over I-5, 2020 Build Alternative traffic would increase by about 100 (in the AM peak hour) to 530 (in the PM peak hour) vehicle trips in comparison to the No Build Alternative, but by only between 240 (in the AM peak hour) to 445 (in the PM peak hour) vehicles in 2040. Based on the predicted level of traffic, the current and newly constructed roadways serving the Thorne Lane interchange would have adequate carrying capacity and are not expected to be impacted by the slight changes in vehicle traffic.

Berkeley Street: At Berkeley Street, the existing bridge over I-5 is proposed to be removed and replaced with a new bridge centerline about 120 feet south of the existing bridge centerline. The new interchange would have roundabouts at the l-5 ramp intersections. The new bridge would extend Jackson Avenue over I-5, the adjacent rail line and Militia Drive. The Jackson Avenue extension would tie into Berkeley Street just west of Washington Avenue, as previously shown in Figure 30. The segment of Berkeley Street east of Union Avenue, including the atgrade railroad crossing near I-5, would be removed. A new residential street would be added and connected to Grant Avenue to provide access for properties along a southern portion of Washington Avenue.

Changes in two-way traffic volumes on local roads near the Berkeley Street interchange are shown in Table 14 for the No Build and Build Alternatives. Two-way traffic along Berkeley Street west of Washington Avenue in 2020 and 2040 is expected to be less than 525 vehicles during the AM and PM peak hours for the No Build and Build Alternatives.

For the portion of Berkeley Street between Union Avenue and Washington Avenue, traffic is generally expected to be reduced with the Build Alternative, as traffic to and from Camp Murray would use the new interchange and the new extension to Jackson Avenue, and would connect to Berkeley Street north of Washington Avenue. However, because of increased
congestion along southbound I-5 during the 2040 PM peak hour, some I-5 southbound drivers would likely exit at Thorne Lane, and use Union Avenue and Berkeley Street to reach their destinations. Traffic along Washington Avenue is expected to be about the same under the No Build Alternative in both 2020 and 2040, and to be less than 140 vehicles.

Table 14: 2020 and 2040 PM Peak Hour Two-way Volumes on Local Streets near the Berkeley Street Interchange - No Build Alternative vs. Build Alternative

| Location | No Build Alternative |  |  |  | Build Alternative |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 2020 |  | 2040 |  | 2020 |  | 2040 |  |
|  | AM | PM | AM | PM | AM | PM | AM | PM |
| Berkeley Street west of Washington Avenue | 415 | 510 | 525 | 450 | 415 | 365 | 445 | 380 |
| Berkeley Street between Union Avenue and Washington Avenue | 460 | 545 | 575 | 515 | 375 | 300 | 385 | 250 |
| Berkeley Street Bridge over I-5 | 1,475 | 1,190 | 1,370 | 1,280 | 1,590 | 1,570 | 1,675 | 1,255 |
| Washington Avenue north of Berkeley Street | 55 | 75 | 70 | 85 | 50 | 75 | 70 | 140 |
| Union Avenue north of Berkeley Street | 380 | 365 | 395 | 500 | 365 | 295 | 375 | 300 |

Traffic volumes crossing l-5 on the new bridge are generally expected to increase with the capacity added by the Build Alternative. An exception would be during the PM peak hour in 2040, when a decrease of about 100 vehicles is expected. Based on the operations analyses of the intersections along these local roads with the Build Alternative, traffic is expected to operate at LOS C or better during both the AM and PM peak hours in 2020 and 2040.

The change in travel patterns would be isolated to a small area of the Tillicum neighborhood, and the subsequent change would not impact or create any adverse conditions on the local roadways. The revised intersection at Berkeley Street/Washington Avenue can be designed to discourage cut-through traffic on Washington Avenue. Possible mitigations can include right-in/right-out operations at the intersection and traffic calming features on Washington Avenue north of Berkeley. The final intersection layout would be designed to discourage both commuter and commercial traffic from using Washington Avenue as a cut-through route to reach destinations beyond the nearby neighborhoods.

Gravelly-Thorne Connector: A new southbound connector road, referred to as the GravellyThorne Connector, is proposed to be constructed to provide a non-freeway connection between Lakewood and the neighborhoods of Tillicum and Woodbrook. Traffic along this new southbound connector road is expected to range from about 25 vehicles (in 2020 AM peak hour) to 75 vehicles (in 2020 PM peak hour). In 2040, traffic along this new southbound connector road is expected to be about 40 vehicles in the AM peak hour and 240 vehicles in
the PM peak hour. Drivers are expected to use this new connector, instead of I-5 or other roads within the secure military installations, to travel from Lakewood to the Tillicum and Woodbrook neighborhoods, Camp Murray, and JBLM. These diversions would be an intended benefit of the proposed Build Alternative. In addition, a new northbound auxiliary lane between the Thorne Lane and Gravelly Lake Drive interchanges would be added, as previously illustrated in Figure 31. This connection offers additional I-5 capacity to accommodate northbound traffic movement between these two interchanges to complement the southbound capacity added by the Gravelly-Thorne Connector.

### 11.0 Transit Service and TDM Activities within the I-5 Study Area

Transit and vanpool service are important factors that affect traffic operations along I-5. The following is a summary of the existing transit service along the l-5 corridor though the JBLM area and the benefits to traffic operations.

### 11.1 Existing Transit Service along I-5

Currently, there are three public transit providers operating within the study area: Intercity Transit, Pierce Transit, and Sound Transit. An illustration of existing transit routes, transit centers and park-and-ride lots within the study area is presented in Figure 57.

Intercity Transit: Based in Thurston County, Intercity Transit (IT) operates five routes through the study area, and subcontracts service for a sixth route. All routes provide access to JBLM through a transfer at the Lakewood Transit Station to
Pierce Transit buses, but none operate directly on the base due to strict security regulations prohibiting general public riders from entering the facility. IT service through the study area includes:

- Route 603 is a weekday route providing bi-directional service between downtown Olympia/Capitol Campus, Lacey (Martin Way park and ride), Lakewood (Lakewood Station/SR 512 park and ride), and Tacoma (Tacoma Dome and downtown).
- Route 605 is a weekday route providing bi-directional service between downtown Olympia/Capitol Campus, Lacey (Martin Way park and ride), Lakewood (Lakewood Station/SR 512 park and ride), and Tacoma (Tacoma Dome and downtown).
- Route 609 is a weekday route providing bi-directional service between Tumwater (state agency campus), Olympia Capitol Campus, Lacey (Hawkes Prairie park and ride), and Lakewood (Lakewood Station/SR 512 park and ride).

Figure 57: Existing Transit Service and Park and Ride Lots


- Route 612 is a weekday route providing bi-directional service between Tacoma (Tacoma Dome and downtown), Lakewood (SR 512 Park and Ride and Lakewood Station), Lacey (Lacey Transit Center), and Olympia (Capitol Campus and downtown).
- Route 620 serves the study area on weekends providing bi-directional service between Olympia (downtown and Capitol Campus), Lacey (Lacey Transit Center and Martin park and ride), Lakewood (Lakewood Station and SR 512 park and ride lot), and Tacoma Mall.

IT contracts with Sound Transit to provide Route 592 weekday service between Olympia and Seattle which is described below under Sound Transit.

IT also offers a commuter vanpool program that serves a wide variety of destinations throughout Thurston, Pierce, Kitsap, Grays Harbor, King, and Lewis counties. Thirty-seven of the more than 230 IT vans currently on the road operate to and from JBLM (including Ft. Lewis, Madigan and McChord) and Camp Murray.

Additional vanpool groups use I-5 with destinations in the cities of Lakewood and DuPont. IT has been in regional discussions with JBLM to consider methods that would serve the general public's need for transit to the bases while satisfying the military's need for base security.

Pierce Transit: Pierce Transit is responsible for local bus service in Pierce County and operates four routes that provide access to or close to JBLM.

- Route 51 connects the Lakewood Station in the vicinity of the Bridgeport Way interchange with the Lakewood
 Transit Center and destinations in central and north Tacoma.
- Route 204 operates via South $112^{\text {th }}$ Street and serves the SR 512 park and ride lot. Service is also available to McChord North Gate at the intersection of South $112^{\text {th }}$ and Tacoma Way/Union Avenue.
- Route 206 operates between the Lakewood Transit Center and Madigan Hospital.
- Route 300 serves JBLM McChord Field operating between the Tacoma Mall Transit Center and McChord Commissary with stops at the SR 512 park and ride lot.

Similar to IT, Pierce Transit also offers regional vanpool services along the I-5 corridor. Currently 31 vans serve JBLM.

Sound Transit: The Central Puget Sound transit provider, Sound Transit (ST), operates three express bus routes along the l-5 corridor within the study area. All service is provided during peak periods in the morning and
evening. ST does not provide local bus service to JBLM. The closest stops are located at the Lakewood Sounder Station and park and ride lot and in DuPont. The Sound Transit routes are:

- Route 574 operates between the Lakewood Transit Center and SeaTac Airport.
- Route 592 (Olympia Express) operates between the Olympia Transit Center and downtown Seattle including the Hawks Prairie park and ride lot, DuPont, Lakewood and the SR 512 park and ride. Since October 2013, service has been contracted by IT and operated by ST.
- Route 594 operates between the Lakewood Sounder Station and Seattle.

ST also operates Sounder Rail Service that connects Seattle and Tacoma with the Lakewood Sounder Station. Sounder service is operated in the former BNSF right of way adjacent to and west of I-5 that is now owed by ST. As part of the Point Defiance Bypass Project, WSDOT will eventually improve the tracks along this corridor for Amtrak Cascades and Coast Starlight services which is expected to relocate from the current Point Defiance route in 2017. ST's LongRange Plan includes the potential for commuter rail service to operate to DuPont (and possibly beyond), as well as to JBLM. Such service would likely require adding a second track within the right of way, grade-separating certain crossings, and locating new station(s) by the gate(s) to/from JBLM. Options for expanding l-5 and reconfiguring the interchanges should anticipate these rail operations and facilities, and not preclude or adversely impact them.

### 11.2 Park and Ride Lots

There are seven primary park and ride lots within or serving the corridor study area. A summary of the park and ride inventory data, including number of parking stalls and utilization is shown in Table 15.

Table 15: Park and Ride Lot Inventory

| Facility/Lot | City | Location | Number of <br> Parking Spaces | Average Daily <br> Utilization |
| :--- | :---: | :---: | :---: | :---: |
| SR 512 | Lakewood | I-5 \& SR 512 | 493 | $93 \%$ |
| Lakewood <br> Sounder Station | Lakewood |  <br> $47^{\text {th }}$ Avenue SW | 600 | $50 \%$ |
| DuPont | DuPont |  <br> Palisade Blvd | 126 | $63 \%$ |
| Martin Way | Lacey | I-5 \& Martin Way | 318 |  |
| Hawks Prairie | Lacey | I-5 \& Hogum Bay Road | 332 | $65 \%$ |
| Centennial Station | Thurston Co. | 6600 Yelm Hwy SE | 110 | $27 \%$ |
| Tumwater | Tumwater | Israel/Bonniewood Rd SE | 30 | $2 \%$ |

Source: Intercity Transit, Pierce Transit and Sound Transit, 2013.

### 10.3 Commute Trip Reduction

In 1991, the Washington State Legislature adopted the Commute Trip Reduction (CTR) Law as a tool to help address the growing traffic congestion problem in the state. The CTR encourages the use of non-single occupant vehicle travel modes for works trip using employer-based programs. In 2006, legislators passed the CTR Efficiency Act, that requires local governments in urban areas with traffic congestion to develop programs to reduce drive-alone trips and vehicle miles traveled per capita.

By 2009, the CTR Program had removed 30,000 vehicles from the states roadways each morning, reducing congestion, air pollution and energy consumption. Traffic delays have been cut by eight percent in the Central Puget Sound region, and rush hour commuters saved about $\$ 59$ each during that year in fuel and time. CTR participants also conserved about 3 million gallons of gasoline in the 2009-2010 biennium and drove 154 million fewer miles in comparison with 2007. (Data from WSDOT's CTR website, December 23, 2013.)

CTR targets workplaces with 100 or more full-time employees in the most congested areas of the state. Employers develop and manage their own programs based on locally-adopted goals for reducing vehicle trips and miles traveled. Statewide there are more than 1,050 worksites and 530,000 commuters participating in the CTR program. Employers regularly report on their programs and jurisdictions report on progress toward meeting drive-alone and Vehicle Miles Travelled (VMT) reduction targets.

As noted previously, within the I-5 JBLM study area there are several active CTR programs that affect travel along I-5. These programs are provided by IT and Pierce Transit, which offer carpool, vanpool and other TDM services. In addition to the vanpool service provided by IT and Pierce Transit, Seattle Metro and JBLM also provide vanpool services that reduce traffic flow along the I-5 corridor.

As the largest employer in Pierce County, JBLM has developed an active CTR program:

- Approximately 125 employees use bus subsidies
- Approximately 375 employees use vanpools from either Pierce Transit or Intercity Transit
(Based on data from Joint Base Lewis-McChord Growth Coordination Plan, The Transpo Group, 2010)

The Department of the Army has a program called the "Mass Transportation Benefit Program" (MTBP) that provides reimbursement for using mass transit (either vanpool or carpool). The MTBP is available to all personnel on base (civilian and military) and is a non-taxable program that subsidizes the use of transit up to $\$ 245$ per month.

### 11.4 Transit Performance

As previously shown in Figure 57, there are twelve existing transit routes that serve the study area, either directly or by accommodating through trips that may otherwise have been made in a single occupant vehicle. Even more significant in terms of reducing demand on I-5 is the level of vanpool activity presently occurring within the study area. The following is an analysis of transit ridership and vanpool activity as it affects I-5 in the study area. The focus of this analysis is the PM peak period, which
 typically has the highest level of congestion of any time period within the corridor.

Transit Ridership on I-5 in the Study Area: Table 16 presents a summary of existing PM peak period (3-6 PM) transit ridership on I-5 in the study area as of November 2013. Currently bus transit service in the area is provided primarily by three agencies: Intercity Transit (serving Olympia and Thurston County), Pierce Transit (serving Tacoma and Pierce County), and Sound Transit (serving the Central Puget Sound region). An additional three trips during this time period are provided by the Bremerton-Kitsap Airporter which directly services JBLM, connecting it with the Sea-Tac Airport.

As indicated in the table, IT is currently providing seventeen bus trips through the study area during the 3:00 PM to 6:00 PM peak period, ten in the northbound direction and seven in the southbound direction. The ten northbound routes carry a total average weekday ridership of 214 persons during the PM peak period. The seven southbound routes carry a total average weekday ridership during the PM peak period of 101 persons. This equates to a total weekday PM peak period average of 315 persons.

Pierce Transit has twenty-two buses serving the study area during the PM peak period, eleven in the northbound direction and eleven southbound. Average total weekday ridership during this time period is 226 persons northbound and 299 southbound for a total of 525 persons.

ST has eight trips serving the study area during this same time period, all of which head southbound. Average weekday PM peak period ridership is 232 persons.

Table 16: Weekday PM Peak Period (3-6 PM) Transit Ridership in the Study Area

|  |  | Number of Buses |  | Ridership |  |
| :--- | :--- | :--- | :---: | :---: | :---: |
| Agency | Route | NB | SB | NB | SB |
| Intercity Transit | Route 603 | 5 |  | 159 |  |
|  | Route 605 |  | 3 |  | 79 |
|  | Route 609 | 4 | 4 | 27 | 22 |
|  | Route 612 | 1 |  | 28 |  |
| Pierce Transit | Route 206 | 5 | 5 | 100 | 160 |
|  | Route 300 | 6 | 6 | 126 | 139 |
| Sound Transit | Route 592 |  | 8 |  | 232 |
| Totals |  | 21 | 26 | 440 | 632 |

Source: Intercity and Pierce Transit, 2013.

The total number of buses providing service on I-5 in the study areas during a typical weekday PM peak period is twenty-one northbound and twenty-six southbound. Total persons using transit in the l-5 corridor during this same time period is 440 northbound and 632 southbound for a total weekday PM peak period ridership of 1,072 persons.

Vanpool Ridership on I-5 in Study Area: Table 17 shows weekday PM peak hour ridership in existing vanpools during the summer of 2013. Only official vanpools sponsored by one of the transit operators providing service in the study area are included in this table. Additional vanpool service is provided by other transit agencies and private employers. Currently, IT sponsors 71 vanpools that serve the study area during the PM peak hour. Twenty-two of these vanpools are traveling in the northbound direction from Thurston County to destinations in Pierce and King Counties. These vanpools carry an average of 205 persons on I-5 during the PM peak hour. Forty-nine of these vanpools are traveling southbound from a variety of destinations to Thurston County. These IT vanpools carry an average of 367 persons on I-5 during the PM peak hour.

Pierce Transit sponsors 16 northbound and 3 southbound vanpools that use I-5 through the study area during the weekday PM peak hour. Vanpool ridership on I-5 during this time period
 is 128 northbound and 24 southbound for a total of 153 persons.

Table 17: Weekday PM Peak Hour (4-5 PM) Vanpool Ridership in Study Area

| Agency | Begin Trip | End Trip | Number of Vanpools |  | Ridership |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | NB | SB | NB | SB |
| Intercity Transit | King County | Thurston County |  | 6 |  | 41 |
|  | Thurston County | King County | 8 |  | 88 |  |
|  | Kitsap County | Thurston County |  | 2 |  | 19 |
|  | Camp Murray | Thurston County |  | 3 |  | 19 |
|  | DuPont | Thurston County |  | 12 |  | 76 |
|  | Gig Harbor | Thurston County |  | 1 |  | 18 |
|  | JBLM/Ft. Lewis | Thurston County |  | 10 |  | 70 |
|  | JBLM/Madigan | Thurston County |  | 9 |  | 79 |
|  | Tacoma | Thurston County |  | 6 |  | 45 |
|  | Thurston County | Pierce County | 14 |  | 117 |  |
| Pierce Transit ${ }^{(1)}$ | Pierce County | JBLM | 16 | 3 | 129 | 24 |
| Totals |  |  | 38 | 52 | 334 | 391 |

${ }^{(1)}$ Only partial ridership data is available, ridership total based on estimated average vanpool ridership.

Impacts of I-5 Congestion on Transit: Existing transit service along l-5 in the study area primarily serves either regional through trips, trips to/from ST's Lakewood Station, or trips to/from the Lakewood Transit Center. With over 62,000 employees, JBLM is the second largest employer in Washington State and is the largest potential transit destination in the study area. However, the secure nature of JBLM limits the effectiveness of regular fixed route transit because buses carrying non-military personnel cannot enter the secure facility or require nonmilitary riders to deboard at the security gate. Currently only two routes serve the base, one to Madigan Hospital and the other to the McChord Commissary.

Unlike fixed route bus service, vanpools and carpools that carry only base personnel do have access to and from JBLM. There are vanpools sponsored by the major transit providers in the area that are currently connecting JBLM with destinations throughout the region. In 2013, vanpools and bus service carried approximately 1,200 people along I-5 during the PM peak hour.

Both transit service and vanpools are impacted by freeway congestion, with existing PM peak travel times exceeding off-peak travel time by 75 percent. With no HOV facilities within the study area to facilitate the advantages of alternative mode choices, buses and vanpools are caught in the same traffic as single-occupant vehicles.

With the proposed Build Alternative, all traffic, including transit, carpools, and vanpools, would have shorter travel time in 2020 as compared to the 2020 No Build Alternative. Travel time savings of 10 to 20 minutes for southbound travelers and 10 to 30 minutes for northbound
travelers for trips between SR 510 and SR 512 along I-5. This allows for better transit reliability through the JBLM area along I-5.

Transit and Vanpooling Benefits to Traffic Operations along I-5: Existing transit and vanpool ridership on $\mathrm{I}-5$ in the study area has a substantial impact on reducing vehicular congestion in the corridor during peak weekday travel periods. As illustrated in Table 18, if existing riders where to switch to individual vehicles, a total of approximately 1,000 vehicles would be added to existing I-5 PM peak hour traffic (approximately 440 northbound and 560 southbound).

Table 18: Benefits of Transit and Vanpooling - Weekdays during 4 to 5 PM Peak Hour

|  |  | Ridership |  | Number of Cars Taken off I-5 |  |
| :--- | :--- | :---: | :---: | :---: | :---: |
| Agency | Mode | NB | SB | NB | SB |
| Intercity Transit | Bus | 89 | 83 | 73 | 68 |
|  | Vanpool | 205 | 367 | 168 | 301 |
| Pierce Transit | Bus | 100 | 96 | 82 | 79 |
|  | Vanpool | 129 | 24 | 106 | 20 |
| Sound Transit | Bus | 11 | 107 | 9 | 88 |
| Totals |  | 534 | 677 | 438 | 555 |

By way of comparison, 560 vehicles represent about 31 percent of the existing maximum per lane capacity in the congested heart of the corridor. Thus, it is reasonable to conclude that the availability of transit and vanpooling options significantly benefits existing highway traffic operations. By making transit more reliable, the proposed Build Alternative can encourage more drivers to switch from single occupancy vehicles to transit buses and vanpools to commute to and from their workplace.

### 11.5 Effect of the Build Alternative on Transit and Transportation Demand Management (TDM) Activities

While changes to the existing level of transit service are not included as part of the proposed Build Alternative, the added general purpose lanes along the I-5 mainline would benefit the operations, speed and reliability of transit and various TDM activities such as vanpooling and ridesharing.

With added travel lanes in the Build Alternative from the Thorne Lane to Steilacoom-DuPont Road interchanges, transit travel times would be improved along with all travel modes in comparison to the No Build Alternative. Speeds would be more stable along I-5 and interchange operations would be improved. With the proposed Build Alternative, transit, carpools, and vanpools, as well as general traffic are expected to have shorter PM peak period travel times in 2020, as compared to the No Build Alternative. Travel time savings would be in the order of four minutes for southbound travelers through the JBLM area. Northbound
travelers could expect about 13 minutes in travel time savings for trips between Center Drive and Gravelly Lake Drive. These shorter travel times allow for better transit reliability and schedule adherence along I-5 through the JBLM area, and would also encourage additional vanpool and carpool activities.

In 2040, northbound travel times along l-5 through the project area would improve with the addition of the near-term facilities included with the proposed Build Alternative, while southbound travel time would increase. As a result, transit service, as well as all traffic, would be affected equally.

### 12.0 Build Alternative Benefits to Bicycle and Pedestrian Travel in the Study Area

The proposed Build Alternative includes a separate shared-use path for bicyclists and pedestrians along l-5 from Steilacoom-DuPont Road to Berkeley Street. In addition, bicycle and pedestrian facilities are included along the Gravelly-Thorne Connector. Bicyclists and pedestrians would be able to travel between DuPont and Lakewood by using local streets from Center Drive to Steilacoom-DuPont Road. They could travel on the new shared-use path to the Tillicum neighborhood, on local streets through Tillicum, and along the Gravelly-Thorne Connector to Lakewood, as previously shown on Figure 32.

The redesigned interchanges at Berkeley Street and Thorne Lane are proposed to have pedestrian and bicycle lanes, with sidewalks or shared-use areas to improve non-motorized access over I-5 and the adjacent rail line, connecting portions of Lakewood with JBLM. The improved connections would allow persons stationed or working at JBLM, but living in adjacent communities, the opportunity to walk or bicycle to their duty station or work activities.

### 13.0 Construction Traffic Effects of the Build Alternative

### 13.1 Closures on I-5 and/or its Existing Interchanges

The redesigned interchanges at Berkeley Street and Thorne Lane would be shifted south of the existing interchanges, which would result in fewer impacts to traffic operations during construction than would reconstruction at existing locations. However, some long-term temporary closures (three to six months) may be needed to rebuild the southbound on- and off-ramps at both interchanges. The current intention is to close the southbound ramps at one interchange at a time, while continuing to provide access to local neighborhoods, Camp Murray, and JBLM via the adjacent interchange. The southbound ramp long-term temporary closures could have the following effects:

- Some drivers are expected to use adjacent interchanges such as Berkeley Street when Thorne Lane is closed or Thorne Lane when Berkeley Street is closed.
- Some drivers may use local streets during these closures.
- Some drivers may change the timing of their trips to avoid peak travel times.

A preliminary analysis was conducted to identify potential impacts associated with the longterm temporary closure of the southbound ramps at the Thorne Lane and Berkeley Street interchanges. Analysis showed that, while some traffic on local streets would be changed, the resulting volumes are well within the capacity that these roadways are designed to accommodate.

Temporary northbound on- and off-ramps would be provided around the interchange construction sites to maintain access to neighborhoods and the military installations. However, nighttime and/or weekend closures may be needed while the new ramps are being connected to the existing street system and to l-5.

Construction plans would be developed to keep three lanes open in both the northbound and southbound direction on I-5 between Thorne Lane and Center Drive during daytime and peak travel hours. I-5 will be narrowed and shifted through the corridor construction zone. In addition, nighttime lane closures would be needed to widen $\mathrm{I}-5$, and to build walls and bridge abutments.

### 13.2 Local Street Closures during Construction

With the Berkeley Street and Thorne Lane interchanges being constructed away from the existing structures, temporary closures of local streets are not expected. However, some short-term lane closures or detours would likely be needed to connect the proposed improvements with the existing street system.

### 13.3 Effects of Construction on Existing Transit Service and Bus Routing

Pierce Transit route \#206 serves the Tillicum and Woodbrook communities as well as Madigan Hospital on JBLM. This route will need to pass through the construction work zones for the Thorne Lane and Berkeley Street interchanges, as well as the l-5 mainline between Gravelly Lake Drive and Berkeley Street. During the temporary closures of southbound ramps at the Thorne Lane and Berkeley Street interchanges, the path of Route 206 will need to be modified. Additionally, all transit service provided by Intercity Transit, Pierce Transit and Sound Transit along the I-5 mainline will need to pass through the construction work zone and may be affected by construction-related activity.

School bus service is currently provided by the Clover Park School District to the Tillicum Elementary School and Woodbrook Middle School. This service would be impacted by construction activity at both the I-5/Thorne Lane and I-5/Berkeley Street interchanges.

### 13.4 Construction Traffic Haul Routes

With secure military installations on both sides of the project area, l-5 would be the primary route used to access the construction sites. SR 512 and SR 510 may also be used to haul construction materials to and from the construction area, depending on the location of material sources, off-site manufacturing areas, and staging areas used by the selected contractor.

### 13.5 Construction Traffic Mitigation

Prior to award of the first construction contract to build the improvements included in the Build Alternative, a Transportation Management Plan (TMP) will be developed. The TMP will define strategies to manage traffic through the project's construction work zones during each construction phase. Transit agencies, local governments, school districts, JBLM, Camp Murray and others as appropriate will be invited to participate in development of the TMP. The TMP will be monitored and amended over time as necessary.

Some suggested mitigation measures that could be implemented to manage construction traffic could include:

- Allowing the contractor to close only one ramp at a time.
- Providing advanced communications to all affected parties about closures including times and dates.
- Signing for detour routes to optimize routing and minimize impacts to residential streets and neighborhoods.
- Adjusted signal timings at adjacent interchanges to account for the added constructiondetour traffic.


## Appendix A Methods \& Assumptions Document

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I-5 Joint Base Lewis-McChord Vicinity Interchange Justification Report \& Environmental Documentation

## Methods \& Assumptions Document

Prepared for: Washington State Department of Transportation

Prepared by: H.W. Lochner, Inc. \& Shea Carr Jewell, Inc.
In association with:
The Transpo Group, Inc. Shannon \& Wilson, Inc.

April 2013

Methods \& Assumptions Document

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## Methods and Assumptions

## 1. Stakeholder Acceptance

"The undersigned parties, including all members of the team from WSDOT, FHWA and the Local Agencies, concur with the Interchange Justification Report Methods and Assumptions for the I5 Joint Base Lewis-McChord Vicinity Interchange Justification Report (I-5 JBLM Vicinity IJR) as presented in this document." The signature pages for each jurisdiction are attached at the back of this document.

## STAKEHOLDER ACCEPTANCE

Joint Base Lewis-McChord

Signature

Title


City of Lakewood

## Signature

Title
$\qquad$
Date

City of DuPont

Signature

Title

Date
Town of Steilacoom

Signature

Title

Date

## Pierce County

## Signature

Title

Date
(1) Participation on the Stakeholders Committee and/or signing of this document does not constitute approval of the I-5 JBLM Vicinity IJR.
(2) All members of the Stakeholder Committee will accept this document as a guide and reference as the study progresses through the various stages of project development. If there are any agreed upon changes to the assumptions in this document a revision will be created, endorsed and signed by all the stakeholders.

Thurston Regional Planning Council

## Signature

Title

Date

## Puget Sound Regional Council



## Signature

Title

## Date

WSDOT - Olympic Region Traffic Office

## Signature

Title

Date

WSDOT - HQ Traffic Office

## Signature

Title

Date


Sighature

Date
WSDOT - HQ Access and Hearings

Signature

Title

Date

FHWA

Signature

Title

Date
(1) Participation on the Stakeholders Committee and/or signing of this document does not constitute approval of the I-5 JBLM Vicinity IJR.
(2) All members of the Stakeholder Committee will accept this document as a guide and reference as the study progresses through the various stages of project development. If there are any agreed upon changes to the assumptions in this document a revision will be created, endorsed and signed by all the stakeholders.

## I-5 JBLM Vicinity IJR Methods \& Assumptions Document

## 2. Introduction and Project Description

Interstate $5(I-5)$ is a national highway of strategic importance as it travels from the US/Mexican Border to the US/Canadian border. It is the primary highway for the movement of goods and people traveling north and south on the west coast of the United States. In Washington, l-5 links key population centers Vancouver, Olympia, Tacoma, Seattle, Everett and Bellingham.

Over the past several years, traffic has increased along the entire I-5 corridor from Mexico to Canada. Within our study area in south Pierce County, traffic has also grown, as Joint Base Lewis-McChord (JBLM) has evolved into a strategic military base, Camp Murray has expanded, and the communities of Lakewood, DuPont and Steilacoom have grown. These area changes have added to the increased through-traffic along the l-5 corridor from Olympia to Seattle. Because of the presence of secured military bases on both sides of I-5, there are no routes to use without extended detours to bypass the military bases. Congestion along I-5 through the JBLM vicinity has become a daily occurrence with ramp traffic backing onto the l-5 mainline causing delays and safety issues.

The I-5 JBLM Vicinity IJR Project will include:

- Development of an I-5 Interstate Corridor Plan from the I-5/Center Drive Interchange to the I5/Gravelly Lake Road Interchange;
- Development of a corridor-wide Interchange Justification Report for revisions to the I-5/Steilacoom-DuPont Road Interchange, I-5/Main Gate Interchange, I-5/Berkeley Street Interchange, and I-5/Thorne Lane Interchange;
- Prioritization of interstate improvements; and
- Preparation of the Environmental Documentation and associated preliminary engineering for highest priority improvements.


## Purpose of the Project

The purpose of this project is to define improvements to relieve traffic congestion on the $\mathrm{I}-5$ corridor in the JBLM vicinity with a focus on M.P. 119 to 124 including the interchanges with Steilacoom-DuPont Road, Main Gate, Berkeley Street, and Thorne Lane. A corridor Interchange Justification Report will be prepared addressing these four interchanges at a minimum. The IJR document will be developed in cooperation with the Federal Highway Administration (FHWA), WSDOT, JBLM, Camp Murray, Puget Sound Regional Council (PSRC), Thurston Regional Planning Council (TRPC), Pierce County, Intercity Transit, Pierce Transit, the Town of Steilacoom, and the cities of Lakewood, DuPont, and Lacey.

This project will then develop the necessary environmental documentation and preliminary engineering for the highest priority element(s) of the preferred solutions, as guided by the stakeholders.

The results of the Interchange Justification Report (IJR) and environmental documentation will enable the project stakeholders to assess options and opportunities to improve the transportation system within the study area, and solicit funds to implement the preferred solution in a logical manner. Specifically, the project will address:

## I-5 JBLM Vicinity IJR <br> Methods \& Assumptions Document

- Relieving congestion on I-5 within the study area;
- Improving local and mainline system efficiency;
- Enhancing mobility;
- Improving safety and operations;
- Increasing transit and TDM opportunities.


## Project Leads and Proponents

- Washington State Department of Transportation
- Federal Highway Administration
- Joint Base Lewis-McCord
- Camp Murray
- City of Lakewood
- Town of Steilacoom
- City of Lacey
- Pierce County
- Puget Sound Regional Council
- Thurston Regional Planning Council
- City of DuPont
- Intercity Transit
- Pierce Transit


## Environmental Document Type

Depending on the selected project(s) and the degree of impacts, we are envisioning a Documented Environmental Classification Summary (DECS) or an Environmental Assessment (EA).

## Level of Documentation

The proposed improvement options likely will include substantial revisions to the existing interchanges. As required by WSDOT's Design Manual Chapter 550 and FHWA, eight specific points will be addressed in the IJR. These policy points are:
(1) Policy Point 1: Need for the Access Point Revision - What are the current and projected needs? Why are the existing access points and the existing or improved local system unable to meet the proposal needs? Is the anticipated demand short or long trip?

- Using the Base Conditions operation analyses for 2013, 2020 and 2040 discuss the intersection and interstate deficiencies in access to the Interstate at the Thorne Lane, Berkeley Street, Main Gate and DuPont-Steilacoom Road interchanges.
- Using the collision analysis, discuss the existing safety issues along I-5 and at the Thorne Lane, Berkeley Street, Main Gate and DuPont-Steilacoom Road interchanges and what it may look like in the future if changes do not occur.
(2) Policy Point 2: Reasonable Alternatives - Describe the reasonable alternatives that have been evaluated.
- Discuss all alternatives developed as part of this IJR and explain how these alternatives met or did not meet the purpose of the improvement.
- Discuss why the selected alternative(s) were carried forward for further development.


## I-5 JBLM Vicinity IJR Methods \& Assumptions Document

(3) Policy Point 3: Operational and Collision Analyses - How will the proposal affect safety and traffic operations at year of opening and design year?

- Discuss the results of the intersection and interstate operational analyses for the opening year (2020) and design year (2040) for the recommended Build Alternatives for this IJR.
- Compare the results of the Build Alternatives with the Base Condition results, including the Thorne Lane, Berkeley Street, Main Gate and Steilacoom interchanges.
- Determine the effect of the Build Alternatives on the I-5 mainline operations and adjacent interchanges at Gravelly Lake Road, and Center Drive Interchanges. If the impacts extend further north and south, also analyze the impacts to Mounts Road Interchange, Bridgeport Way Interchange and the SR 512 Interchange.
- Discuss the collision analysis results for the Build Condition as compared to the Base Condition for the opening and design years.
- Discuss impacts to safety and operation of I-5.
(4) Policy Point 4: Access Connections and Design - Will the proposal provide fully directional interchanges connected to public streets or roads, spaced appropriately, and designed to full design level geometric control criteria?
- Discuss the geometric designs of the proposed improvements and show that all movements are included in the design.
- Prepare conceptual horizontal and vertical alignments showing the existing l-5 mainline, proposed ramps and existing cross roads for the selected alternative.
- Discuss design criteria, including ROW and access impacts.
(5) Policy Point 5: Land Use and Transportation Plans - Is the proposed access point revision compatible with all land use and transportation plans for the area?
- Summarize how current land use assumptions are included in the travel demand model.
- Discuss the improvement consistency with local, regional, and statewide transportation plans.
(6) Policy Point 6: Future Interchanges - Is the proposed access point revision compatible with a comprehensive network plan? Is the proposal compatible with other known new access points and known revisions to existing points?
- Discuss the improvement consistency with other planned interstate improvements included in the State-wide Highway System Plan and refer to a future interstate master plan, including impacts of the Cross-Base highway.


## I-5 JBLM Vicinity IJR <br> Methods \& Assumptions Document

(7) Policy Point 7: Coordination - Are all coordinating projects and actions programmed and funded?

- Discuss plans of the local jurisdictions to provide other local improvements to support the interstate modifications and that they will commit to work with WSDOT to pursue funds for the interchange modifications.
- Discuss any previous commitments between agencies or private entities; i.e. financial, environmental, etc.
(8) Policy Point 8: Environmental Processes - What is the status of the proposal's environmental processes? This section should be something more than just a status report of the environmental process; it should be a brief summary of the environmental process.
- Discuss the environmental findings, such as endangered species, priority habitats, wetlands and streams in the area and what environmental permits may be needed to implement the improvements.
- Discuss any known social issues that could affect this proposal.
- Discuss any known or potential hazardous contamination in the area.
- Discuss (if necessary) if the location is within a non-attainment area for air quality.
- Discuss that the environmental process must have WSDOT approval prior to the final IJR approval.


## 3. Analysis Years/Periods

Operational analysis will include AM, Midday and PM peak hours for the following years:

- Existing Base Year - 2013
- Assumed Opening Year - 2020
- Horizon/Design Year - 2040

A sensitivity analysis will also be conducted to assess approximately ten percent higher through traffic volumes along l-5 to account for increased Friday afternoon or Sunday evening situations.

## 4. Project Study Area

The project study area for this I-5 JBLM Vicinity IJR will extend from the I-5/Center Drive Interchange on the south to the I-5/Gravelly Lake Road Interchange on the north as illustrated on Figure 1. This area will include the following intersections for analyses:

- Center Drive Interchange (Exit \#118)
- Northbound Ramps
- (JBLM outbound gate)
- Southbound Ramps
- Wilmington Drive/Center Drive
- DuPont-Steilacoom Road Interchange
(Exit \#119)
- Northbound Ramps
- Southbound Ramps
- Wilmington Dr./Barksdale Ave.
- Main Gate Interchange (Exit \# 120)
- Northbound Ramps
- Southbound Ramps
- JBLM Gates
- Berkeley Street Interchange (Exit \#122)
- Northbound Ramps
- Southbound Ramps
- Union Avenue/Berkeley Street
- Thorne Lane Interchange (Exit \#123)
- Northbound Ramps
- Southbound Ramps
- Union Avenue/Thorne Lane
- Gravelly Lake Drive Interchange (Exit \#124)
- Northbound Ramps
- Southbound Ramps
- Pacific Highway S/Gravelly Lake Dr.

If the traffic analyses and the volumes changes show that there are impacts to adjacent interchanges further north or south, then they will be included in the project impact analysis, including:

- Mounts Road Interchange (Exit \#116)
- Northbound Ramps
- Southbound Ramps
- SR 512 Interchange (Exit \#127)
- Southbound Off-ramp
- Bridgeport Way Interchange (Exit \#125)
- Northbound Ramps
- Southbound Ramps
- Pacific Highway S/Bridgeport Way

The study area for the travel demand model will include most of Pierce County and the north portion of Thurston County.

## 5. Traffic Operations Analysis

For interstate highway operations, the 2010 Highway Capacity Manual (HCM) using the associated Highway Capacity software (HCS) (version 6.4) will be used to analyze mainline, merge/diverge connections and weaves situations. Average vehicle speed and density will be used as performance measures for the HCS analysis. For the three analysis years, AM, Midday and PM peak hour analyses will be performed.

For ramp terminal/surface street operations, intersections will be analyzed as follows:

- Synchro 8.0 software will be used to analyze the operations of signalized intersections.
- Synchro 8.0 software or HCS will be used to analyze unsignalized intersections.
- SIDRA 5.1 software package using standard model with HCS on will be used to analyze roundabout controlled intersections.
- SimTraffic software will be used to check Synchro results for ramp queuing.

For the preferred alternative, a simulation model capable of analyzing freeway and geometry between intersections and interchanges, including weaving sections and multiple vehicle classes will be used. VISSIM was selected for the simulation of the preferred alternative because it meets these needs while also providing animation graphics. The following VISSIM simulations will be prepared:

- Existing Year 2013 PM Peak Period (for model calibration)


## I-5 JBLM Vicinity IJR Methods \& Assumptions Document

- Design Year 2040 PM Peak Period for the Base Conditions
- Design Year 2040 PM Peak Period for the preferred alternative
- Design Year 2013 AM Peak Period (for model calibration)
- Design Year 2040 AM Peak Period for the Base Conditions
- Design Year 2040 AM Peak Period for the preferred alternative

For this report, the operational analysis area will include the l-5 corridor between Mounts Road and SR 512 interchanges and all ramp terminals.

## 6. Travel Forecast

The existing I-5/JBLM/Lakewood model developed for the l-5 Alternatives Analysis Study and consistent with the PSRC regional model will be utilized to develop forecasts for 2020 (year of opening) and 2040 (design year). In addition, the recent results and modeling efforts completed for the Lacey Area IJR will be used to help reconcile the differences between the PSRC and TRPC travel demand forecasts. This will include a more refined post-processing effort and rationale in balancing the vehicle demand and trips entering and exiting the Pierce/Thurston County line.

The 2020 model will include all local and regionally funded improvements and the 2040 model will include projects adopted in the region's Metropolitan Transportation Plan. Travel forecasts for the AM, mid-day, and PM peak periods and hours will be prepared.

## Model Overview

The I-5/JBLM/Lakewood model was selected as the preferred model because it was specifically developed to support evaluation of I-5 mainline and interchange concepts in the JBLM vicinity. The available models in the area such as the PSRC, Pierce County, and TRPC models were not sufficiently refined in and around JBLM, Camp Murray, DuPont, and Lakewood to allow for the level of detail needed for an accurate assessment of I-5 and the area's transportation system. The I-5/JBLM/Lakewood model is a refined version of Pierce County's regional EMME model, but has been converted to the VISUM software platform. Transportation Analysis Zones (TAZs) have been subdivided to better model traffic patterns in the area and between major subareas of JBLM. Travel characteristics specific to the area have been introduced along with specific trip purposes and distribution for JBLM related travel to better model each of the interchanges and installation points of entry.

The model study area includes most of Pierce County, and some major highways and arterials in northeastern Thurston County. The base year model will be calibrated for AM, mid-day, and PM peak periods based on traffic counts collected during those times. Model parameters (screen lines, trip distribution, time-of day, etc.) will be validated based on FHWA guidelines. Consistency with PSRC and TRPC assumptions will be part of the model validation process. Given the recent work that has been competed for the Lacey Area IJR, the model calibration and post-processing will be sensitive to the travel forecast imbalance between the Pierce and Thurston county boundaries. The IJR team will work closely with TRPC and PSRC to solidify the model results to ensure a more accurate representation of

## I-5 JBLM Vicinity IJR <br> Methods \& Assumptions Document

future travel characteristics are developed for this study. Testing of future scenarios will be conducted to review model sensitivity to changes in travel demand or the model network.

## Freeway Traffic Forecasts

Forecasts will be developed for SOV and HOV classes of vehicles. Truck volumes will be estimated based upon available truck counts and existing truck percentages. HOV 2+ and HOV 3+ trip tables will be prepared based on PSRC model assumptions for each of the model time periods. In regards to transit, the VISUM model will not provide direct model data for transit vehicles, but it will be flexible to transitrelated assumptions. The person-trip mode-split factors come from the PSRC model, and future year mode splits will reflect PSRC anticipated changes to transit in the future. For the I-5 JBLM specific zones, adjustments can be made to the mode split or time-of-day factors based on various transit scenario assumptions. The effect on traffic volumes will be scaled accordingly.

## Interchange \& Intersection Traffic Forecasts

Future interchange and intersection traffic volumes will be developed using travel forecasts from the model. The model travel forecasts for each time period will be post-processed and translated into vehicle volumes for use in the operations analysis. The interchange and intersection volumes will be balanced using the freeway ramp volumes as control totals.

## 7. Highway Network Assumptions

The following baseline conditions are assumed:

- 2013 Base Conditions
- Existing Highway Network
- 2020 Base Conditions
- Funded Tiger III Improvements
- Funded TIP improvements from Local Jurisdictions
- Funded STIP improvements
- Funded JBLM Improvements
- Funded rail improvements
- Funded inter-regional transit and vanpool service
- 2040 Base Conditions
- Same as 2020 Base Conditions.
- Cross-Base Highway is not included as part of the base conditions.
- Modified 2040 Base with Unfunded Local Improvements
- Local Improvements from the Long Range Regional Transportation Plan will be reviewed by the technical support group and selected improvements will be included.
- Cross-Base Highway improvement will be analyzed for conditions with and without the corridor.


## I-5 JBLM Vicinity IJR <br> Methods \& Assumptions Document

## 8. Build Highway Network Assumptions

- Build Alternatives 2020
- Use same local highway network as developed for the 2020 Base Conditions.
- Modify I-5 mainlines and ramps as approved by Stakeholders
- Build Alternatives 2040
- Use same local highway network as developed for the Modified 2040 Base Conditions with and without the Cross-Base Highway.
- Modify I-5 mainlines and ramps as approved by Stakeholders


## 9. Safety Issues

This IJR will use the current Collision Analysis Location/Collision Analysis Corridor (CAL/CAC) criteria and the Intersection Analysis Location (IAL) criteria for state highways within the project area. In addition, the collision rates along local streets will be estimated using available local collision data. Types of accidents and contributing factors to collisions will also be summarized by location. The most recent five years of available collision data will be used for this analysis. This corridor-specific information as well as statewide system collision statistics will be used in a predictive collision analysis effort to estimate any change in the level of safety for the interstate and connecting roadways.

Procedures developed in the Highway Safety Manual will be investigated for potential use in predicting future safety assessments of the preferred Build Alternative.

## 10. Deviations/Justifications

At this point in the process, there are no deviations identified. Deviations may be indentified through the various study results, and will be documented as they arise.

## 11. Selection of Measures of Effectiveness (MOE)

The metrics to be used to demonstrate how the proposal will accomplish the stated objectives will be aligned with the provisions outlined in the Moving Washington initiative. These metrics may include but not be limited to the following:

1. Traffic Operations along I-5 (Travel time and density)
2. Traffic Operations at ramp terminals (Average intersection delay and $95 \%$ queue lengths)
3. Impacts critical environmental habitat (Area impacted).
4. Safety Analysis Results (Accident Potential/Risk Reduction).
5. Travel time savings for freight movement
6. Reduction in SOV trips (identify goal) through increased TDM and transit ridership
7. Effect of "Managed Lanes" compared to general purpose (peak period SOV)
8. Design Standards/Deviations
9. Right of Way/Access Impacts

## Methods \& Assumptions Document

The list of criteria will be finalized as the evaluation methodology is developed with approval of the Stakeholders.

## 12. Resolution of Late Comments

From time to time, ideas or suggestions arise late in the evaluation or documentation process. Some of these late emerging ideas may have merit and added benefits to the project, but be difficult to incorporate in the on-going process. It is understood that new ideas may bring value to the final outcomes and therefore should not be automatically dismissed because of the sequence of events and timing of the information. Specific protocols will be in place to allow new ideas and information to be "vetted" and reviewed for consideration, as follows:

If new ideas and information are brought forward, they will be first discussed between WSDOT's Project Manager and the Consultant's Project Manager who will determine its merits. If they decide that the new idea has merit it will be referred to WSDOT/FHWA Core Team to decide how the new idea should be addressed in the IJR and environmental process. If the WSDOT and Consultant Project Managers decide that the idea has little merit, it will be added under policy point 2, if appropriate, and addressed as an idea considered.

For ideas that have already been considered and dismissed, but there is new interest in reconsideration, the WSDOT's Project Manager and the Consultant's Project Manager will determine if reintroducing the idea has merits. If they decide that the new idea has merit the idea will be referred to WSDOT/FHWA Core Team to decide how the revised idea should be addressed in the IJR and environmental process.

If a new idea and/or prior information is brought forward during a stakeholder meeting, the content of this information will not be fully discussed if it impacts the scheduled agenda. The Consultant's Project Manager will note the comments and content of the information and will assure that review of the new information will follow the approved protocols for consideration.

A log of all late ideas and suggestions will be maintained by the Consultant's Project Manager who will briefly summarize the idea or concept and show its status.

## 13. Conclusion

This study will review and analyze options for improving access to the Interstate system without degrading the mainline freeway or off-ramp operations and safety. While degradation of the Interstate system is not an acceptable outcome, there may be localized areas where degradation may occur due to system tradeoffs. Engineering judgment will be applied to arrive at the best overall set of improvements practical within the study area. This will be accomplished by thoroughly evaluating specific MOEs that are in alignment with the stated goals and the Moving Washington initiative.

[^2]

Methods \& Assumptions Document

Interchange Justification Report \& Environmental Documentation

## Stakeholder Acceptance

"The undersigned party, in partnership with all members of the team from WSDOT, FHWA and the Local Agencies, concur with the Methods \& Assumptions Document for the l-5 Joint Base Lewis-McChord Vicinity Interchange Justification Report (I-5 JBLM Vicinity IJR) as presented in this document."


Signature


Date
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9 May 2013
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## I-5 JBLM Vicinity IJR Methods \& Assumptions Document

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Thurston Regional Planning Council


Title
July 11, 2013
Date
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Puget Sound Regional Councip

Signature

Director of Integrated Planning
Title

July 11, 2013
Date
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## Relation Aoministectienz

Title

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WSDOT - Olympic Region Traffic

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## WSDOT - HQ Access and Hearings



Date 28,1013
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## Federal Highway Administration



Signature

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## Appendix B

## Summary of Intersection Turning Movement Volumes

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Post-processed Data
from Mesoscopic Model










Post-processed Data
from Mesoscopic Model




| Post－processed Data from Mesoscopic Model | Post－Processed <br> EXISTING <br> 2013 Model Volumes <br> Peak Hour |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| North－South Street East－West Street | $\begin{gathered} 3 \\ 2013 \\ \hline \end{gathered}$ | Center Dr Wilmington Dr |  |  |  |  |
| Count Date：3／5／2013 | 80 <br> 70 |  | \％ |  |  | $\begin{gathered} 335 \\ 210 \end{gathered}$ |
| Count Source：TC2 |  |  | $\stackrel{\square}{8}$ | 8 |  |  |
| eb wb nb sb total |  | 1，795 |  |  | 90 |  |
| \％HV 0\％0\％1\％1\％ |  |  |  |  | 25 |  |
| PHF 0.98 |  |  |  |  | 220 |  |
| Peak Hour Used： |  | \％ | 号 | $\stackrel{\text { ¢ }}{\sim}$ |  |  |
| From 1630 To 1730 |  | $\stackrel{\text { ¢ }}{\infty}$ |  | $\stackrel{\square}{\sim}$ |  |  |
| North－South Street East－West Street | $\begin{gathered} 4 \\ 2013 \\ \hline \end{gathered}$ |  | Center Dr <br> SB I－5 Ramps |  |  |  |
| Count Date：3／5／2013 |  |  | $\stackrel{セ 0}{\sim}$ |  |  | 3450 |
| Count Source：TC2 |  |  | ®ㅜㄹ |  |  |  |
| eb Wb nb Sb Total |  | 2，040 |  |  | 345 |  |
| \％HV 1\％0\％1\％ |  |  |  |  | 0 |  |
| PHF 0.97 |  |  |  |  | 0 | 0 |
| Peak Hour Used： |  | 喡 | $\stackrel{\circ}{0}$ |  |  |  |
| From 1630 To 1730 |  | ลิ | $\stackrel{\circ}{\infty}$ |  |  |  |







| Post－processed Data from Mesoscopic Model | Post－Processed EXISTING <br> 2013 Model Volumes <br> Peak Hour |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| North－South Street East－West Street | $\begin{array}{\|c} \hline 7 \\ 2013 \\ \hline \end{array}$ | $\begin{array}{r} \text { Steilac } \\ \mathrm{s}: \\ \hline \end{array}$ | －5 Ra | $\overline{\text { ont Rd }}$ |  |  |
| Count Date：2／14／2013 |  | \％ |  | 웃 |  |  |
| Count Source：TC2 |  | $\stackrel{\sim}{\circ}$ | 年 |  |  |  |
| eb wb nb sb Total | 865 |  |  |  | 165 | 185 |
| \％HV 10\％1\％4\％ |  |  | 2，090 |  | 0 |  |
| PHF 0.97 | 0 |  |  |  | 20 | 0 |
| Peak Hour Used： |  | 岩 | $\stackrel{\text { \＆}}{0}$ |  |  |  |
| From 1630 To 1730 |  | 莓 |  | $\begin{aligned} & \text { 읃 } \\ & \hline \end{aligned}$ |  |  |
| North－South Street East－West Street | $\begin{array}{\|c\|} \hline 8 \\ 2013 \end{array}$ | Steilac | －5 Ra | ont Rd |  |  |
| Count Date：2／14／2013 |  | 岁 |  | $\stackrel{\text { 年 }}{\sim}$ |  |  |
| Count Source：TC2 |  |  | ゅ | $\stackrel{\circ}{7}$ |  |  |
| EB WB NB SB Total | 0 | 400 |  |  |  | 0 |
| \％HV $2 \% \quad 0 \% \quad 3 \%$ |  | 10 | 2，020 |  |  |  |
| PHF 0.97 | 635 | 225 |  |  |  | 605 |
| Peak Hour Used： |  |  | $\stackrel{\text { ® }}{ }$ | $\stackrel{\infty}{\square}$ |  |  |
| From 1630 To 1730 |  | 응 |  | \％ |  |  |




















# Appendix C No Build Alternative Intersection Analysis Summary 

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Intersection Analysis Summary - 2020 No Build


Intersection Analysis Summary - 2020 No Build

|  |  |  |  |  |  |  | M PEA | HOUR |  |  |  |  | M PEA | HOUR |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| No. | Intersection | Control Type | Approach Road | Movement | Post- <br> Process Volume (vph) | LOS | Delay (sec) <br> oach | LOS | Delay (sec) <br> Movem | 95th <br> Queue <br> (ft) <br> nt | Post- <br> Process Volume (vph) | LOS <br> Ap | Delay (sec) <br> oach | LOS | Delay (sec) <br> Movem | 95th Queue <br> (ft) <br> nt |
|  |  |  |  | Overall | 2,130 | E | 72.6 |  |  |  | 2,020 | B | 19.5 |  |  |  |
|  |  |  | Barksdale Avenue | SB-L | 20 |  |  | E | 61.5 | 43 | 40 |  |  | C | 34.4 | 62 |
|  |  |  | Barksdale Avenue | SB-T | 65 | D | 47.0 | D | 43.7 | 104 | 85 | C | 32.2 | C | 31.4 | 121 |
|  | DuPont- |  | Barksdale Avenue | SB-R | 20 |  |  | D | 73.7 | 104 | 25 |  |  | C | 31.4 | 121 |
|  | Steilacoom |  | Steilacoom-DuPont | NB-L | 240 |  |  | D | 39.7 | m189 | 190 |  |  | C | 27.2 | 194 |
|  | Road / |  | Steilacoom-DuPont | NB-T | 65 | F | 74.7 | C | 28.3 | m41 | 105 | C | 23.1 | C | 21.3 | 105 |
| 8 | Barksdale | Signal | Steilacoom-DuPont | NB-R | 905 |  |  | F | 87.3 | m247 | 310 |  |  | C | 21.2 | 67 |
|  | Avenue / |  | Wilmington Drive | EB-L | 10 |  |  | D | 38.2 | 25 | 35 |  |  | C | 30.3 | 52 |
|  | Wilmington |  | Wilmington Drive | EB-T | 60 | B | 17.6 | D | 38.2 | 91 | 100 | A | 7.5 | C | 33.2 | 119 |
|  | Drive |  | Wilmington Drive | EB-R | 80 |  |  | A | 0.1 | 0 | 485 |  |  | A | 0.5 | 0 |
|  |  |  | Steilacoom-DuPont | WB-L | 590 |  |  | F | 85.1 | \#500 | 575 |  |  | C | 24.6 | 305 |
|  |  |  | Steilacoom-DuPont | WB-T | 60 | F | 85.1 | F | 85.2 | \#506 | 40 | C | 24.6 | C | 24.5 | 303 |
|  |  |  | Steilacoom-DuPont | WB-R | 15 |  |  | F | 85.2 | \#506 | 30 |  |  | C | 24.5 | 303 |
|  |  |  |  | Overall | 2,310 |  |  |  |  |  | 2,985 |  |  |  |  |  |
|  |  |  | 1-5 Off Loop Ramp | EB-R | 305 |  |  |  |  |  | 50 |  |  |  |  |  |
|  |  | Cloverleaf | 1-5 Off-Ramp | WB-R | 75 |  |  |  |  |  | 25 |  |  |  |  |  |
| 11 | Division Drive | Merge / | 41st Division Drive | NB-T | 450 |  | icable |  |  |  | 1,400 |  |  |  |  |  |
|  | (Ma |  | 41st Division Drive | NB-R | 260 |  |  |  |  |  | 435 |  |  |  |  |  |
|  |  |  | 41st Division Drive | SB-T | 920 |  |  |  |  |  | 655 |  |  |  |  |  |
|  |  |  | 41st Division Drive | SB-R | 300 |  |  |  |  |  | 420 |  |  |  |  |  |
|  |  |  |  | Overall | 2,050 |  |  |  |  |  | 2,960 |  |  |  |  |  |
|  |  |  | 1-5 Off Loop Ramp | EB-R | 120 |  |  |  |  |  | 50 |  |  |  |  |  |
|  | / 41st | Cloverleaf | $1-5$ Off-ramp | WB-R | 390 |  |  |  |  |  | 50 |  |  |  |  |  |
| 12 | Division Drive | Merge / | 41st Division Drive | NB-T | 320 |  |  |  | ro AI |  | 690 |  | icable |  | hro An |  |
|  | (Main Gate) |  | 41st Division Drive | NB-R | 205 |  |  |  |  |  | 735 |  |  |  |  |  |
|  |  |  | 41st Division Drive | SB-T | 830 |  |  |  |  |  | 1,025 |  |  |  |  |  |
|  |  |  | 41st Division Drive | SB-R | 185 |  |  |  |  |  | 410 |  |  |  |  |  |
|  |  |  |  | Overall | 2,545 | C | 23.5 |  |  |  | 2,445 | C | 20.4 |  |  |  |
|  |  |  | 1-5 Off-ramp | EB-L | 170 |  |  | F | 91.3 | \#262 | 85 |  |  | E | 60.0 | 124 |
|  |  |  | 1 -5 Off-ramp | EB-T | 0 | C | 20.3 |  |  |  | 5 | E | 56.9 | E | 60.0 | 124 |
|  |  |  | 1-5 Off-ramp | EB-R | 620 |  |  | A | 0.8 | 0 | 5 |  |  | A | 0.0 | 0 |
| 13 | / Berklely | Signal | Berkeley Ave | NB-L | 0 |  |  |  |  |  | 0 |  |  |  |  |  |
| 13 | /Berklely | Signal | Berkeley Ave | NB-T | 235 | D | 54.7 | E | 60.0 | 336 | 480 | B | 17.9 | D | 53.2 | \#516 |
|  |  |  | Berkeley Ave | NB-R | 450 |  |  | D | 52.0 | 111 | 1,195 |  |  | A | 3.6 | 0 |
|  |  |  | Berkeley Ave | SB-L | 55 |  |  | A | 5.8 | 104 | 190 |  |  | C | 21.4 | 128 |
|  |  |  | Berkeley Ave | SB-T | 1,015 | A | 5.8 | A | 5.8 | 104 | 485 | C | 21.4 | C | 21.4 | 128 |
|  |  |  | Berkeley Ave | SB-R | 0 |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  | Overall | 1,675 | D | 42.8 |  |  |  | 1,510 | C | 33.9 |  |  |  |
|  |  |  | 1-5 Off-ramp | WB-L | 905 |  |  | D | 47.9 | 578 | 405 |  |  | E | 65.0 | \#282 |
|  |  |  | 1-5 Off-ramp | WB-T | 0 | D | 44.4 |  |  |  | 5 | E | 63.7 | E | 63.0 | \#274 |
|  |  |  | 1 -5 Off-ramp | WB-R | 140 |  |  | C | 29.4 | 45 | 5 |  |  | C | 42.6 | 0 |
| 14 | / Berklely | Signal | Berkeley Ave | NB-L | 125 |  |  | C | 30.3 | 153 | 300 |  |  | B | 13.8 | 84 |
|  |  |  | Berkeley Ave | NB-T | 280 | C | 30.3 | C | 30.3 | 153 | 265 | B | 13.8 | B | 13.8 | 84 |
|  |  |  | Berkeley Ave | NB-R | 0 |  |  |  |  |  | 0 |  |  |  |  |  |
|  |  |  | Berkeley Ave | SB-L | 0 |  |  |  |  |  | 0 |  |  |  |  |  |
|  |  |  | Berkeley Ave | SB-T | 165 | E | 57.5 | E | 59.7 | 257 | 270 | C | 32.1 | D | 43.8 | 288 |
|  |  |  | Berkeley Ave | SB-R | 60 |  |  | D | 51.4 | 35 | 260 |  |  | D | 35.4 | 67 |
| 15 | Berklely <br> Avenue / <br> Union <br> Avenue | All-way Stop Control |  | Overall | 790 | B | 11.7 |  |  |  | 860 | B | 14.4 |  |  |  |
|  |  |  | Militia Dr | EB-L | 5 | A | 9.9 | A | 9.9 | 2 | 0 | A | 8.8 |  |  |  |
|  |  |  | Militia Dr | EB-T | 5 |  |  | N | 9.5 | - | 0 |  |  |  |  |  |
|  |  |  | Militia Dr | EB-R | 0 |  |  |  |  |  | 5 |  |  | A | 8.8 | 0 |
|  |  |  | Union Ave | WB-L | 115 | B | 11.1 | B | 12.0 | 15 | 125 | B | 11.1 | B | 11.8 | 20 |
|  |  |  | Union Ave | WB-T | 5 |  |  | A | 9.0 | 6 | 5 |  |  | A | 8.8 | 4 |
|  |  |  | Union Ave | WB-R | 45 |  |  | A | 9.0 | 6 | 30 |  |  | A | 8.8 | 4 |
|  |  |  | Berkeley Ave | NB-L | 5 | B | 12.2 | B | 14.0 | 60 | 0 | A | 9.2 |  |  |  |
|  |  |  | Berkeley Ave | NB-T | 285 |  |  | A | 9.6 | 25 | 90 |  |  | A | 9.3 | 10 |
|  |  |  | Berkeley Ave | NB-R | 200 |  |  | A | 9.6 | 25 | 180 |  |  | A | 9.2 | 20 |
|  |  |  | Berkeley Ave | SB-L | 10 | B | 10.9 | B | 10.9 | 25 | 25 | C | 19.0 | C | 19.0 | 102 |
|  |  |  | Berkeley Ave | SB-T | 110 |  |  | B | 10.9 | 25 | 400 |  |  | C | 19.0 | 102 |
|  |  |  | Berkeley Ave | SB-R | 5 |  |  |  |  |  | 0 |  |  |  |  |  |

Intersection Analysis Summary - 2020 No Build

|  |  | Control Type | Approach Road | Movement | AM PEAK HOUR |  |  |  |  |  | PM PEAK HOUR |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| No. | Intersection |  |  |  | Post- <br> Process <br> Volume (vph) | LOS <br> Ap | Delay <br> (sec) <br> roach | LOS | Delay (sec) <br> Movem | 95th <br> Queue <br> (ft) <br> nt | Post- <br> Process <br> Volume (vph) | LOS <br> Ap | Delay <br> (sec) <br> roach | LOS | Delay <br> (sec) <br> Movem | 95th <br> Queue <br> (ft) <br> nt |
| 17 | Berklely <br> Avenue/ Washington Avenue | Two-way Stop Control on Washington Avenue |  | Overall | 470 | B | 12.6 |  |  |  | 570 | B | 12.4 |  |  |  |
|  |  |  | Washington Ave | EB-L | 0 | A | 8.8 |  |  |  | 0 | B | 10.8 |  |  |  |
|  |  |  | Washington Ave | EB-T | 0 |  |  |  |  |  | 0 |  |  |  |  |  |
|  |  |  | Washington Ave | EB-R | 5 |  |  | A | 8.8 | 0 | 5 |  |  | B | 10.8 | 0 |
|  |  |  | Washington Ave | WB-L | 35 | B | 12.6 | B | 12.6 | 10 | 25 | B | 12.4 | B | 12.4 | 6 |
|  |  |  | Washington Ave | WB-T | 0 |  |  |  |  |  | 0 |  |  |  |  |  |
|  |  |  | Washington Ave | WB-R | 5 |  |  | B | 12.6 | 10 | 15 |  |  | B | 12.4 | 6 |
|  |  |  | Berkeley Ave | NB-L | 5 | A | 0.1 | A | 7.4 | 0 | 5 | A | 0.3 | A | 8.2 | 0 |
|  |  |  | Berkeley Ave | NB-T | 320 |  |  | A | 0.0 |  | 90 |  |  | A | 0.0 |  |
|  |  |  | Berkeley Ave | NB-R | 10 |  |  | A | 0.0 |  | 25 |  |  |  | 0.0 |  |
|  |  |  | Berkeley Ave | SB-L | 5 | A | 0.4 | A | 8.0 | 0 | 10 | A | 0.2 | A | 7.5 | 0 |
|  |  |  | Berkeley Ave | SB-T | 85 |  |  | A | 0.0 |  | 395 |  |  | A | 0.0 |  |
|  |  |  | Berkeley Ave | SB-R | 0 |  |  |  |  |  | 0 |  |  |  |  |  |
| 18 | I-5 NB Ramps / Thorne Lane | Signal |  | Overall | 1,490 | D | 35.8 |  |  |  | 1,930 | D | 38.4 |  |  |  |
|  |  |  | 1-5 Off-ramp | EB-L | 15 | D | 44.9 | D | 44.3 | 32 | 10 | D | 43.7 | D | 43.3 | 31 |
|  |  |  | $1-5$ off-ramp | EB-T | 0 |  |  | D | 44.3 | 32 | 5 |  |  | D | 43.8 | 64 |
|  |  |  | 1 -5 off-ramp | EB-R | 215 |  |  | D | 45.0 | 65 | 175 |  |  | D | 43.8 | 64 |
|  |  |  | Thorne Ln | NB-L | 0 | E | 56.9 |  |  |  | 0 | D | 54.9 |  |  |  |
|  |  |  | Thorne Ln | NB-T | 355 |  |  | E | 71.1 | \#482 | 400 |  |  | E | 74.0 | \#499 |
|  |  |  | Thorne Ln | NB-R | 255 |  |  | D | 37.0 | 61 | 645 |  |  | D | 43.1 | 232 |
|  |  |  | Thorne Ln | SB-L | 230 | B | 12.7 | B | 12.7 | m115 | 370 | B | 12.1 | B | 12.1 | 145 |
|  |  |  | Thorne Ln | SB-T | 420 |  |  | B | 12.7 | m115 | 325 |  |  | B | 12.1 | 145 |
|  |  |  | Thorne Ln | SB-R | 0 |  |  |  |  |  | 0 |  |  |  |  |  |
| 19 | I-5 SB Ramps/ Thorne Lane | Signal |  | Overall | 1,380 | E | 55.4 |  |  |  | 1,705 | D | 45.4 |  |  |  |
|  |  |  | 1 -5 off-ramp | WB-L | 400 | E | 58.2 | E | 77.2 | \#540 | 235 | D | 48.7 |  |  |  |
|  |  |  | 1 -5 Off-ramp | WB-T | 5 |  |  | E | 77.2 | \#540 | 10 |  |  | E | 59.7 | \#334 |
|  |  |  | 1 -5 Off-ramp | WB-R | 315 |  |  | C | 33.4 | 61 | 575 |  |  | D | 44.0 | 121 |
|  |  |  | Thorne Ln | NB-L | 245 | D | 43.8 | C | 25.9 | m155 | 375 | C | 26.0 | C | 26.0 | m150 |
|  |  |  | Thorne Ln | NB-T | 125 |  |  | C | 25.9 | m155 | 35 |  |  | C | 26.0 | m150 |
|  |  |  | Thorne Ln | NB-R | 0 |  |  |  |  |  | 0 |  |  |  |  |  |
|  |  |  | Thorne Ln | SB-L | 0 | F | 102.9 |  |  |  | 0 | E | 56.4 |  |  |  |
|  |  |  | Thorne Ln | SB-T | 250 |  |  | F | 93.3 | \#373 | 460 |  |  | E | 57.2 | \#915 |
|  |  |  | Thorne Ln | SB-R | 40 |  |  | D | 40.4 | 0 | 15 |  |  | C | 30.5 | 0 |
| 20 | Union Ave / Union Avenue Loop | Tee with Stop Sign on Union Avenue |  | Overall | 730 | B | 10.4 |  |  |  | 1,090 | B | 11.6 |  |  |  |
|  |  |  | Union Ave | EB-L |  | B | 10.4 |  |  |  |  | B | 11.6 |  |  |  |
|  |  |  | Union Ave | EB-T |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  | Union Ave | EB-R | 125 |  |  | B | 10.4 | 15 | 190 |  |  | B | 11.6 | 20 |
|  |  |  | Thorne Ln | NB-L | 230 | - | 4.4 | A | 8.4 | 15 | 330 | - | 4.8 | A | 8.9 | 20 |
|  |  |  | Thorne Ln | NB-T | 210 |  |  | A | 0.0 | - | 280 |  |  | A | 0.0 |  |
|  |  |  | Thorne Ln | NB-R | 0 |  |  |  |  |  | 0 |  |  |  |  |  |
|  |  |  | Thorne Ln | SB-L | 0 | - | 0.0 |  |  |  | 0 | - | 0.0 |  |  |  |
|  |  |  | Thorne Ln | SB-T | 165 |  |  | - | - | - | 285 |  |  |  |  |  |
|  |  |  | Thorne Ln | SB-R | 0 |  |  |  |  |  | 5 |  |  |  |  |  |
| 22 | I-5 NB Ramps / Gravelly Lake Drive | Signal |  | Overall | 1,355 | C | 27.8 |  |  |  | 1,695 | D | 41.6 |  |  |  |
|  |  |  | $1-5$ Off-ramp | EB-L | 460 | D | 48.7 | D | 53.5 | \#449 | 745 | E | 64.6 | E | 65.1 | \#714 |
|  |  |  | 1 -5 Off-ramp | EB-T | 0 |  |  |  |  |  | 5 |  |  | E | 64.1 | \#701 |
|  |  |  | $1-5$ Off-ramp | EB-R | 110 |  |  | D | 43.8 | \#309 | 65 |  |  | E | 64.1 | \#701 |
|  |  |  | Gravelly Lk Dr | NB-L | 0 | D | 48.6 |  |  |  | 0 | E | 67.3 |  |  |  |
|  |  |  | Gravelly Lk Dr | NB-T | 130 |  |  | D | 48.6 | 93 | 205 |  |  | E | 67.3 | 178 |
|  |  |  | Gravelly Lk Dr | NB-R | 40 |  |  | D | 48.6 | 93 | 45 |  |  | E | 67.3 | 178 |
|  |  |  | Gravelly Lk Dr | SB-L | 580 | A | 2.7 | A | 2.8 | m21 | 560 | A | 1.7 | A | 1.9 | m1 |
|  |  |  | Gravelly Lk Dr | SB-T | 35 |  |  | A | 0.1 | m0 | 70 |  |  | A | 0.1 | m0 |
|  |  |  | Gravelly Lk Dr | SB-R | 0 |  |  |  |  |  | 0 |  |  |  |  |  |

Intersection Analysis Summary - 2020 No Build

| No. | Intersection | Control Type | Approach Road | Movement | AM PEAK HOUR |  |  |  |  |  | PM PEAK HOUR |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  | Post- <br> Process Volume (vph) | LOS <br> Ap | Delay (sec) <br> oach | LOS | Delay <br> (sec) <br> Movem | 95th <br> Queue <br> (ft) <br> nt | Post- <br> Process <br> Volume <br> (vph) | LOS <br> Ap | Delay (sec) <br> oach | LOS | Delay <br> (sec) <br> Movem | 95th <br> Queue <br> (ft) <br> nt |
| 23 | I-5 SB Ramps/ GravellyLake Drive | Signal |  | Overall | 2,120 | D | 39.3 |  |  |  | 2,480 | D | 37.2 |  |  |  |
|  |  |  | 1-5 Off-ramp | WB-L | 5 | D | 48.1 | D | 46.1 | 15 | 10 | E | 62.7 |  |  |  |
|  |  |  | 1 -5 Off-ramp | WB-T | 0 |  |  |  |  |  | 0 |  |  | E | 61.0 | 29 |
|  |  |  | 1 -5 Off-ramp | WB-R | 355 |  |  | D | 48.1 | 91 | 340 |  |  | E | 62.7 | 103 |
|  |  |  | Gravelly Lk Dr | NB-L | 60 | A | 7.0 | A | 7.0 | 44 | 40 | A | 8.4 |  |  |  |
|  |  |  | Gravelly Lk Dr | NB-T | 510 |  |  | A | 7.0 | 44 | 910 |  |  | A | 8.4 | 86 |
|  |  |  | Gravelly Lk Dr | NB-R | 0 |  |  |  |  |  | 0 |  |  |  |  |  |
|  |  |  | Gravelly Lk Dr | SB-L | 0 | D | 52.7 |  |  |  | 0 | D | 52.8 |  |  |  |
|  |  |  | Gravelly Lk Dr | SB-T | 610 |  |  | E | 56.6 | \#764 | 620 |  |  | E | 57.4 | \#894 |
|  |  |  | Gravelly Lk Dr | SB-R | 580 |  |  | D | 48.5 | 259 | 560 |  |  | D | 47.7 | 408 |
| 25 | Gravelly Lake Drive / Pacific Highway | Signal |  | Overall | 2,370 | C | 33.0 |  |  |  | 2,840 | D | 37.1 |  |  |  |
|  |  |  | Pacific Hwy | WB-L | 90 | D | 53.2 | D | 54.1 | 63 | 250 | E | 68.3 | E | 71.1 | 175 |
|  |  |  | Pacific Hwy | WB-T | 0 |  |  |  |  |  | 0 |  |  |  |  |  |
|  |  |  | Pacific Hwy | WB-R | 125 |  |  | D | 52.5 | 60 | 150 |  |  | E | 63.5 | 132 |
|  |  |  | Gravelly Lk Dr | NB-L | 0 | D | 47.5 |  |  |  | 0 | B | 13.7 |  |  |  |
|  |  |  | Gravelly Lk Dr | NB-T | 825 |  |  | D | 47.9 | 361 | 1,125 |  |  | B | 14.8 | 174 |
|  |  |  | Gravelly Lk Dr | NB-R | 40 |  |  | D | 40.1 | m19 | 125 |  |  | A | 4.1 | m7 |
|  |  |  | Gravelly Lk Dr | SB-L | 190 | C | 19.8 | B | 14.9 | 138 | 260 | D | 51.2 | D | 41.0 | 295 |
|  |  |  | Gravelly Lk Dr | SB-T | 1,100 |  |  | C | 20.7 | 437 | 930 |  |  | D | 54.1 | 542 |
|  |  |  | Gravelly Lk Dr | SB-R | 0 |  |  |  |  |  |  |  |  |  |  |  |

Note: For Two-way Stop Control InterscetionS - Overall LOS and delay is based on worse approach/movement
Signalized and Non-signalized intersections analyzed with Synchro software
Rounadabout interscetion analyzed with Sidra software

Intersection Analysis Summary - 2040 No Build


Intersection Analysis Summary - 2040 No Build

|  |  |  |  |  |  |  | M PEA | HOUR |  |  |  |  | M PEA | HOU |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| No. | Intersection | Control Type | Approach Road | Movement | Post- <br> Process Volume (vph) | LOS Ap | Delay (sec) <br> oach | LOS | Delay <br> (sec) <br> Movem | 95th <br> Queue <br> (ft) <br> nt | Post- <br> Process <br> Volume <br> (vph) | LOS | Delay (sec) <br> oach | LOS | Delay <br> (sec) <br> Movem | 95th <br> Queue <br> (ft) <br> nt |
|  |  |  |  | Overall | 2,490 | F | 125.0 |  |  |  | 2,420 | C | 20.9 |  |  |  |
|  |  |  | Barksdale Avenue | SB-L | 25 |  |  | D | 44.6 | 42 | 50 |  |  | C | 35.3 | 62 |
|  |  |  | Barksdale Avenue | SB-T | 75 | D | 37.5 | C | 35.7 | 105 | 100 | C | 33.2 | C | 32.3 | 113 |
|  |  |  | Barksdale Avenue | SB-R | 25 |  |  | C | 35.7 | 105 | 20 |  |  | C | 32.3 | 113 |
|  |  |  | Steilacoom-DuPont | NB-L | 265 |  |  | C | 31.1 | 248 | 180 |  |  | C | 31.0 | 159 |
| 8 |  |  | Steilacoom-DuPont | NB-T | 75 | F | 166.6 | B | 17.7 | 69 | 90 | C | 25.8 | C | 23.5 | 80 |
|  |  |  | Steilacoom-DuPont | NB-R | 1,070 |  |  | F | 210.6 | \#824 | 435 |  |  | C | 24.1 | 73 |
|  |  |  | Wilmington Drive | EB-L | 15 |  |  | C | 31.2 | 28 | 25 |  |  | C | 26.3 | 35 |
|  |  |  | Wilmington Drive | EB-T | 165 | C | 23.9 | D | 39.8 | 175 | 180 | A | 7.9 | C | 31.6 | 168 |
|  |  |  | Wilmington Drive | EB-R | 115 |  |  | A | 0.1 | 0 | 675 |  |  | A | 0.9 | 0 |
|  |  |  | Steilacoom-DuPont | WB-L | 580 | F | 97.7 | F | 100.5 | \#473 | 590 | C | 29.7 | C | 29.6 | \#350 |
|  |  |  | Steilacoom-DuPont | WB-T | 60 | F | 97.7 | C | 94.8 | \#469 | 50 | C | 29.7 | C | 29.8 | \#356 |
|  |  |  |  | Overall | 2,380 |  |  |  |  |  | 2,880 |  |  |  |  |  |
|  |  |  | 1-5 Off Loop Ramp | EB-R | 355 |  |  |  |  |  | 45 |  |  |  |  |  |
|  |  | Cloverleaf | 1-5 Off-Ramp | WB-R | 135 |  |  |  |  |  | 50 |  |  |  |  |  |
| 11 | Division Drive | Merge / | 41st Division Drive | NB-T | 515 |  |  |  |  |  | 1,270 |  | plicable |  |  |  |
|  | (M |  | 41st Division Drive | NB-R | 305 |  |  |  |  |  | 440 |  |  |  |  |  |
|  |  |  | 41st Division Drive | SB-T | 855 |  |  |  |  |  | 620 |  |  |  |  |  |
|  |  |  | 41st Division Drive | SB-R | 215 |  |  |  |  |  | 455 |  |  |  |  |  |
|  |  |  |  | Overall | 2,000 |  |  |  |  |  | 2,950 |  |  |  |  |  |
|  |  |  | 1-5 Off Loop Ramp | EB-R | 290 |  |  |  |  |  | 180 |  |  |  |  |  |
|  |  | Clo | 1-5 Off-ramp | WB-R | 75 |  |  |  |  |  | 100 |  |  |  |  |  |
| 12 |  | Merge / | 41st Division Drive | NB-T | 405 |  |  |  |  |  | 630 |  |  |  |  |  |
|  | (M |  | 41st Division Drive | NB-R | 245 |  |  |  |  |  | 690 |  |  |  |  |  |
|  |  |  | 41st Division Drive | SB-T | 780 |  |  |  |  |  | 895 |  |  |  |  |  |
|  |  |  | 41st Division Drive | SB-R | 205 |  |  |  |  |  | 455 |  |  |  |  |  |
|  |  |  |  | Overall | 2,610 | B | 12.9 |  |  |  | 2,505 | B | 16.3 |  |  |  |
|  |  |  | 1-5 Off-ramp | EB-L | 205 |  |  | E | 78.1 | \#286 | 115 |  |  | D | 49.3 | 157 |
|  |  |  | 1-5 Off-ramp | EB-T | 0 | C | 20.1 |  |  |  | 5 | D | 38.1 |  |  |  |
|  |  |  | 1-5 Off-ramp | EB-R | 615 |  |  | A | 0.8 | 0 | 35 |  |  | A | 0.0 | 0 |
| 13 | / Berklely | Signal | Berkeley Ave | NB-L | 0 |  |  |  |  |  | 0 |  |  |  |  |  |
|  |  |  | Berkeley Ave | NB-T | 280 | C | 20.0 | E | 56.4 | \#361 | 500 | B | 17.0 | D | 46.2 | \#562 |
|  |  |  | Berkeley Ave | NB-R | 525 |  |  | A | 0.6 | 0 | 1,185 |  |  | A | 4.7 | 0 |
|  |  |  | Berkeley Ave | SB-L | 70 |  |  |  |  |  | 235 |  |  |  |  |  |
|  |  |  | Berkeley Ave | SB-T | 915 | A | 1.0 | A | 1.0 | 21 | 430 | A | 9.3 | A | 9.3 | 80 |
|  |  |  | Berkeley Ave | SB-R | 0 |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  | Overall | 1,790 | D | 38.4 |  |  |  | 1,605 | C | 27.6 |  |  |  |
|  |  |  | 1-5 Off-ramp | WB-L | 825 |  |  | D | 52.1 | \#505 | 350 |  |  | D | 50.4 | \#263 |
|  |  |  | 1-5 Off-ramp | WB-T | 0 | D | 47.1 |  |  |  | 5 | D | 47.5 | D | 50.4 | \#254 |
|  |  |  | 1-5 Off-ramp | WB-R | 235 |  |  | C | 29.1 | 49 | 80 |  |  | D | 36.9 | 35 |
| 14 | / Berklely | Signal | Berkeley Ave | NB-L | 120 |  |  | B | 16.3 | 105 | 350 |  |  | A | 6.7 | 32 |
|  | Avenue |  | Berkeley Ave | NB-T | 365 | B | 16.3 | B | 16.3 | 105 | 265 | A | 6.7 | A | 6.7 | 32 |
|  |  |  | Berkeley Ave | NB-R | 0 |  |  |  |  |  | 0 |  |  |  |  |  |
|  |  |  | Berkeley Ave | SB-L | 0 |  |  |  |  |  | 0 |  |  |  |  |  |
|  |  |  | Berkeley Ave | SB-T | 160 | D | 44.8 | D | 47.7 | 201 | 315 | D | 35.1 | D | 39.1 | \#367 |
|  |  |  | Berkeley Ave | SB-R | 85 |  |  | D | 39.4 | 43 | 240 |  |  | C | 29.7 | 66 |
| 15 | Berklely <br> Avenue / <br> Union <br> Avenue | All-way Stop Control |  | Overall | 920 | C | 15.2 |  |  |  | 965 | C | 19.6 |  |  |  |
|  |  |  | Militia Dr | EB-L | 5 | B | 10.3 | B | 10.3 | 10 | 0 | A | 10.0 |  |  |  |
|  |  |  | Militia Dr | EB-T | 5 |  |  | B | 10.3 | 10 | 0 |  |  |  |  |  |
|  |  |  | Militia Dr | EB-R | 0 |  |  |  |  |  | 10 |  |  | A | 10.0 | 0 |
|  |  |  | Union Ave | WB-L | 120 | B | 11.8 | B | 12.8 | 61 | 200 | C | 16.1 | C | 17.4 | 70 |
|  |  |  | Union Ave | WB-T | 5 |  |  | A | 9.4 | 17 | 5 |  |  | A | 9.6 | 12 |
|  |  |  | Union Ave | WB-R | 45 |  |  |  |  |  | 35 |  |  | A | 9.6 | 12 |
|  |  |  | Berkeley Ave | NB-L | 5 | C | 17.1 | C | 20.9 | 111 | 0 | B | 12.3 | B | 11.1 | 38 |
|  |  |  | Berkeley Ave | NB-T | 385 |  |  | A | 9.9 | 18 | 110 |  |  | B | 12.9 | 23 |
|  |  |  | Berkeley Ave | NB-R | 210 |  |  |  |  |  | 235 |  |  |  |  |  |
|  |  |  | Berkeley Ave | SB-L | 10 | B | 11.7. | B | 11.7 | 39 | 25 | D | 29.0 | D | 29.0 | 127 |
|  |  |  | Berkeley Ave | SB-T | 125 |  |  |  |  |  | 345 |  |  | D | 29.0 | 127 |
|  |  |  | Berkeley Ave | SB-R | 5 |  |  |  |  |  | 0 |  |  |  |  |  |

Intersection Analysis Summary - 2040 No Build

|  |  | Control Type | Approach Road | Movement | AM PEAK HOUR |  |  |  |  |  | PM PEAK HOUR |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| No. | Intersection |  |  |  | Post- <br> Process <br> Volume <br> (vph) | LOS <br> Ap | Delay <br> (sec) <br> roach | LOS | Delay (sec) <br> Movem | 95th <br> Queue <br> (ft) <br> nt | Post- <br> Process <br> Volume (vph) | LOS <br> Ap | Delay <br> (sec) <br> roach | LOS | Delay <br> (sec) <br> Movem | 95th <br> Queue <br> (ft) <br> nt |
| 17 | Berklely <br> Avenue/ Washington Avenue | Two-way Stop Control on Washington Avenue |  | Overall | 590 | B | 14.3 |  |  |  | 520 | B | 12.2 |  |  |  |
|  |  |  | Washington Ave | EB-L |  | A | 8.8 |  |  |  |  | B | 10.4 |  |  |  |
|  |  |  | Washington Ave | EB-T |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  | Washington Ave | EB-R | 5 |  |  | A | 8.8 | 0 | 5 |  |  | B | 10.4 | 0 |
|  |  |  | Washington Ave | WB-L | 40 | B | 14.3 | B | 14.3 | 8 | 25 | B | 12.2 | B | 12.2 | 5 |
|  |  |  | Washington Ave | WB-T |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  | Washington Ave | WB-R | 10 |  |  | B | 14.3 | 8 |  |  |  |  |  |  |
|  |  |  | Berkeley Ave | NB-L | 5 |  | 0.1 | A | 7.4 | 0 | 5 |  | 0.1 | A | 8.0 |  |
|  |  |  | Berkeley Ave | NB-T | 415 |  |  |  | 0.0 |  | 340 |  |  |  | 0.0 |  |
|  |  |  | Berkeley Ave | NB-R | 15 |  |  |  | 0.0 |  |  |  |  |  |  |  |
|  |  |  | Berkeley Ave | SB-L | 5 |  | 0.4 | A | 8.3 | 0 | 5 |  | 0.3 | A | 7.5 |  |
|  |  |  | Berkeley Ave | SB-T | 95 |  |  | A | 0.0 |  | 95 |  |  |  | 0.0 |  |
|  |  |  | Berkeley Ave | SB-R |  |  |  |  |  |  | 45 |  |  |  | 0.0 |  |
| 18 | I-5 NB Ramps / Thorne Lane | Signal |  | Overall | 1,735 | C | 31.7 |  |  |  | 1,820 | C | 34.8 |  |  |  |
|  |  |  | 1-5 Off-ramp | EB-L | 10 | D | 48.5 | D | 48.1 | 25 | 10 | D | 48.8 | D | 48.3 | 32 |
|  |  |  | $1-5$ off-ramp | EB-T | 0 |  |  |  |  |  | 5 |  |  | D | 48.3 | 32 |
|  |  |  | 1 -5 off-ramp | EB-R | 225 |  |  | D | 48.5 | 66 | 320 |  |  | D | 48.9 | 78 |
|  |  |  | Thorne Ln | NB-L | 0 | D | 47.0 |  |  |  | 0 | D | 52.4 |  |  |  |
|  |  |  | Thorne Ln | NB-T | 445 |  |  | E | 60.5 | \#596 | 395 |  |  | E | 72.0 | \#559 |
|  |  |  | Thorne Ln | NB-R | 345 |  |  | C | 29.7 | 101 | 400 |  |  | C | 33.1 | 92 |
|  |  |  | Thorne Ln | SB-L | 275 | A | 9.1 |  |  |  | 355 | A | 7.6 |  |  | m97 |
|  |  |  | Thorne Ln | SB-T | 435 |  |  | A | 9.1 | m90 | 335 |  |  | A | 7.6 |  |
|  |  |  | Thorne Ln | SB-R | 0 |  |  |  |  |  | 0 |  |  |  |  |  |
| 19 | I-5 SB Ramps/ Thorne Lane | Signal |  | Overall | 1,555 | E | 56.0 |  |  |  | 1,435 | D | 45.0 |  |  |  |
|  |  |  | $1-5$ off-ramp | WB-L | 395 | E | 69.7 | E | 101.0 | \#594 | 240 | E | 60.1 | F | 86.7 | \#397 |
|  |  |  | 1 -5 Off-ramp | WB-T | 5 |  |  | E | 101.0 | \#594 | 10 |  |  | F | 86.7 | \#397 |
|  |  |  | 1 -5 Off-ramp | WB-R | 340 |  |  | C | 32.9 | 69 | 320 |  |  | D | 39.3 | 76 |
|  |  |  | Thorne Ln | NB-L | 325 | A | 4.5 | A | 4.5 | m55 | 355 | A | 4.7 | A | 4.7 | m51 |
|  |  |  | Thorne Ln | NB-T | 130 |  |  | A | 4.5 | m55 | 50 |  |  | A | 4.7 | m51 |
|  |  |  | Thorne Ln | NB-R | 0 |  |  |  |  |  | 0 |  |  |  |  |  |
|  |  |  | Thorne Ln | SB-L | 0 | F | 92.8 |  |  |  | 0 | E | 61.7 |  |  |  |
|  |  |  | Thorne Ln | SB-T | 315 |  |  | F | 101.2 | \#489 | 450 |  |  | E | 62.5 | \#612 |
|  |  |  | Thorne Ln | SB-R | 45 |  |  | C | 34.1 | 4 | 10 |  |  | C | 24.5 | 0 |
| 20 | Union Ave / Union Avenue Loop | Tee with Stop Sign on Union Avenue |  | Overall | 830 | B | 11.2 |  |  |  | 835 | B | 12.8 |  |  |  |
|  |  |  | Union Ave | EB-L |  | B | 11.2 |  |  |  |  | B | 12.8 |  |  |  |
|  |  |  | Union Ave | EB-T |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  | Union Ave | EB-R | 140 |  |  | B | 11.2 | 20 | 160 |  |  | B | 12.8 | 18 |
|  |  |  | Thorne Ln | NB-L | 250 | - | 4.6 | A | 8.7 | 20 | 220 |  | 5.4 | A | 9.0 | 14 |
|  |  |  | Thorne Ln | NB-T | 220 |  |  | A | 0.0 |  | 150 |  |  | A | 0.0 |  |
|  |  |  | Thorne Ln | NB-R |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  | Thorne Ln | SB-L |  | - | 0.0 |  |  |  |  |  | 0.0 |  |  |  |
|  |  |  | Thorne Ln | SB-T | 220 |  |  |  |  |  | 300 |  |  |  |  |  |
|  |  |  | Thorne Ln | SB-R |  |  |  |  |  |  | 5 |  |  |  |  |  |
| 22 | I-5 NB Ramps / Gravelly Lake Drive | Signal |  | Overall | 1,490 | C | 33.0 |  |  |  | 1,820 | D | 50.4 |  |  |  |
|  |  |  | 1-5 Off-ramp | EB-L | 505 | E | 57.8 | E | 63.2 | \#544 | 720 | E | 56.7 | E | 57.2 | \#654 |
|  |  |  | 1 -5 Off-ramp | EB-T | 0 |  |  |  |  |  | 5 |  |  | E | 57.2 | \#654 |
|  |  |  | 1-5 Off-ramp | EB-R | 110 |  |  | D | 52.2 | \#395 | 60 |  |  | E | 56.1 | \#638 |
|  |  |  | Gravelly Lk Dr | NB-L | 0 | E | 58.8 |  |  |  | 0 | F | 103.8 |  |  |  |
|  |  |  | Gravelly Lk Dr | NB-T | 140 |  |  | E | 58.8 | 120 | 350 |  |  | F | 108.3 | \#344 |
|  |  |  | Gravelly Lk Dr | NB-R | 45 |  |  | E | 58.8 | 120 | 90 |  |  | F | 108.3 | \#344 |
|  |  |  | Gravelly Lk Dr | SB-L | 685 | A | 4.0 | A | 4.1 | m29 | 565 | A | 2.7 | A | 2.9 | m2 |
|  |  |  | Gravelly Lk Dr | SB-T | 5 |  |  | A | 0.0 | m0 | 30 |  |  | A | 0.1 | m0 |
|  |  |  | Gravelly Lk Dr | SB-R | 0 |  |  |  |  |  | 0 |  |  |  |  |  |

Intersection Analysis Summary - 2040 No Build

| No. | Intersection | Control Type | Approach Road | Movement | AM PEAK HOUR |  |  |  |  |  | PM PEAK HOUR |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  | Post- <br> Process Volume (vph) | LOS $\underbrace{$ Delay  <br> $(\mathrm{sec})$}$_{\text {Approach }}$ |  | LOS | Delay 95th <br> (sec) |  | Post- <br> Process <br> Volume (vph) | LOS $\underset{\text { Approach }}{$ Delay  <br>  (sec) $}$ |  | LOS | Delay (sec) | 95th <br> Queue <br> (ft) |
| 23 | I-5 SB Ramps <br> / Gravelly <br> Lake Drive | Signal |  | Overall | 2,345 | D | 43.3 |  |  |  | 2,520 | D | 41.5 |  |  |  |
|  |  |  | 1 -5 Off-ramp | WB-L | 5 | E | 57.0 | E | 55.3 | 17 | 5 | E | 58.1 | E | 56.5 | 17 |
|  |  |  | 1 -5 Off-ramp | WB-T | 0 |  |  |  |  |  | 0 |  |  | E | 56.5 | 17 |
|  |  |  | 1-5 Off-ramp | WB-R | 305 |  |  | E | 57.1 | 93 | 295 |  |  | E | 58.1 | 90 |
|  |  |  | Gravelly Lk Dr | NB-L | 70 |  |  | A | 4.7 | 36 | 120 |  |  |  |  |  |
|  |  |  | Gravelly Lk Dr | NB-T | 575 | A | 4.7 | A | 4.7 | 36 | 950 | A | 9.0 | A | 9.0 | m87 |
|  |  |  | Gravelly Lk Dr | NB-R | 0 |  |  |  |  |  | 0 |  |  |  |  |  |
|  |  |  | Gravelly Lk Dr | SB-L | 0 |  |  |  |  |  | 0 |  |  |  |  |  |
|  |  |  | Gravelly Lk Dr | SB-T | 685 | E | 58.1 | E | 72.9 | \#958 | 590 | E | 67.4 | F | 88.6 | \#857 |
|  |  |  | Gravelly Lk Dr | SB-R | 705 |  |  | D | 43.7 | 477 | 560 |  |  | D | 45.1 | 339 |
| 25 | Gravelly Lake Drive / Pacific Highway | Signal |  | Overall | 2,640 | D | 36.6 |  |  |  | 2,720 | D | 47.6 |  |  |  |
|  |  |  | Pacific Hwy | WB-L | 125 | D | 43.1 | D | 44.1 | 70 | 210 | E | 67.7 | E | 70.5 | 150 |
|  |  |  | Pacific Hwy | WB-T | 0 |  |  |  |  |  | 0 |  |  |  |  |  |
|  |  |  | Pacific Hwy | WB-R | 145 |  |  | D | 42.3 | 58 | 185 |  |  | E | 64.4 | 135 |
|  |  |  | Gravelly Lk Dr | NB-L | 0 | E | 61.9 |  |  |  | 0 | D | 52.4 |  |  |  |
|  |  |  | Gravelly Lk Dr | NB-T | 830 |  |  | E | 63.9 | \#425 | 1,125 |  |  | D | 54.6 | 638 |
|  |  |  | Gravelly Lk Dr | NB-R | 50 |  |  | C | 28.2 | 37 | 120 |  |  | C | 31.3 | 86 |
|  |  |  | Gravelly Lk Dr | SB-L | 225 | C | 20.4 | B | 14.1 | 138 | 140 | C | 34.9 | C | 27.0 | 158 |
|  |  |  | Gravelly Lk Dr | SB-T | 1,265 |  |  | C | 21.5 | 448 | 940 |  |  | D | 36.0 | 541 |
|  |  |  | Gravelly Lk Dr | SB-R | 0 |  |  |  |  |  |  |  |  |  |  |  |

Note: For Two-way Stop Control InterscetionS - Overall LOS and delay is based on worse approach/movement
Signalized and Non-signalized intersections analyzed with Synchro software
Rounadabout interscetion analyzed with Sidra software

## Appendix D <br> Summary of l-5 Mainline and Ramp Volumes

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## 2013 AM PEAK HOUR - PO - EXISTING CONDITIONS -- VOLUMES -- MESO - ALL MODE - Post Processed





## l-5 Mainline and Ramp Volumes

## 2020 AM PEAK HOUR - P1 - BASE CONDITIONS WITH TIP IMPROVEMENTS -- VOLUMES -- MESO - ALL MODE - Post Processed





## l-5 Mainline and Ramp Volumes

## 2040 AM PEAK HOUR - P1 - BASE CONDITIONS WITH TIP IMPROVEMENTS -- VOLUMES -- MESO - ALL MODE - Post Processed





I-5 Mainline and Ramp Volumes

## 2020 AM PEAK HOUR - REVISED BUILD ALTERNATIVE IMPROVEMENTS -- VOLUMES -- MESO - ALL MODE - Post Processed



2020 PM PEAK HOUR - REVISED BUILD ALTERNATIVE IMPROVEMENTS -- VOLUMES -- MESO - ALL MODE - Post Processed



I-5 Mainline and Ramp Volumes

## 2040 AM PEAK HOUR - REVISED BUILD ALTERNATIVE IMPROVEMENTS -- VOLUMES -- MESO - ALL MODE - Post Processed





# Appendix E <br> Description of Alternative Packages 

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## Description of the Phase 2 Alternative Packages

The alternative packages evaluated as part of the Phase 2 study effort are described below.

## P1: No Action Alternative - 2020 and 2040:

The No Action Alternative in 2020 and 2040 is similar to the 2013 existing conditions with the addition of TIGER III Grant projects and the Madigan Access Improvements, as well as projects affecting the area from TIP and STIP programs. In addition, there are other off-I-5 improvements including various JBLM gate changes. Both the opening of the new Integrity Gate and modifications to the Mounts Road Gate may affect traffic volumes at the I-5 interchanges.

Transit service enhancements identified in PSRC's Transportation 2040 regional plan are also assumed to be in place in this alternative. These enhancements focus primarily on the long-term plans of Sound Transit and include the extension of Sounder Commuter Rail to DuPont. For 2020, existing transit service is assumed.

## P2: Enhanced Transit Alternative - 2020 and 2040:

This package contains all elements of the P1 - No Action Alternative. It would also add enhanced transit service including the following new bus routes with 15 -minute headways during peak commute periods:

- Lacey to DuPont P\&R to Main Gate to Lakewood
- Lacey to Yelm to East Gate to Spanaway or Puyallup
- Lacey to SR 512 park-and-ride lot to Downtown Tacoma
- Spanaway to Lakewood to Lacey
- Lacey to Main Gate to Lakewood

These new routes represent what would essentially be a doubling of existing service along the I-5 corridor. Alternative P2 also assumes an expanded shuttle bus system on JBLM that matches the offBase transit schedule, thus facilitating a smooth and connected trip to and from the base.

P3: Alternative with Local Road Improvements with Enhanced Transit Service - 2020 and 2040: This package contains all elements of the P2 - Enhanced Transit Alternative and would also include the following local road improvements, as illustrated in Figure 1:

- B-3: Gravelly Lake Connector - Add a new 2-lane urban road west of and parallel to l-5 between Thorne Lane and Gravelly Lake Drive.
- B-13: SR 507 - Widen 507 to four lanes from McKenna to East Gate Road.
- B-17: New High Speed Road - Construct a new highway/high speed arterial road from the Joint Base Connector Road to 176th Street SE.
- C-7: South A Road Extension - Extend South A Road from Jackson Road to Logistics Gate.
- C-8: Joint Base Connector Phase 2 - Add a new 4-lane higher speed connection between Lewis Main and McChord Field.
- C-9: Fairway Road Extension - Improve and extend Fairway Road as 2-lane road from the new Joint Base Connector to Bridgeport Way.
- C-15b: New arterial - Add a two-lane urban road close to the l-5 corridor, from Mounts Road to Jackson Avenue.
- C-21: New JBLM Collector Street, DuPont Gate to East Gate - Construct or improve a new twolane road, following the rail alignment and combat vehicle trail.
- C-30: On-Base Signalization Improvements - Synchronize existing traffic signal operations in the Pendleton Avenue/Jackson Avenue corridor.


## P4: I-5 Express Lanes Alternative - 2020 and 2040:

Alternative P4 would add two l-5 express lanes in each direction. The express lanes would extend from north of the Center Drive Interchange to north of the Gravelly Lake Drive Interchange. These express lanes would be 'managed lanes' and can evolve over time to best address demand, technology, and future conditions. Some possible options for the managed lanes could include: congestion pricing, High Occupancy Vehicle (HOV) lane(s), High Occupancy and Toll (HOT) lane(s), "truck only" lane(s), and/or "smart car only" lane(s).

For analysis purposes, it was assumed that the express lanes would include an HOV lane and a GP lane in each direction. For the 2020 analysis, one of the existing GP lanes north of the Gravelly Lake Drive Interchange was assumed to be converted to an HOV lane. In the 2040 configuration, an HOV lane would be added to the existing four GP lanes north of Thorne Lane and would be added to the existing three lanes at the south end of the project into Thurston County.

P4a: I-5 Express Lanes Alternative with Local Road Improvements - 2020 and 2040:
This alternative package would include all the improvements in the P4 - Express Lane Alternative and would add the three local road improvements listed below:

- B-3: Gravelly Lake Connector - A new 2-lane urban road west of and parallel to I-5 between Thorne Lane and Gravelly Lake Drive
- C-8: Joint Base Connector - A new 4-lane higher speed connection between Fort Lewis and McChord Field.
- C-9: Fairway Road Extension - Improve and extend Fairway Road as 2-lane road from the new Joint Base Connector to Bridgeport Way.

These local improvements would provide alternative on-Base and off-Base local routes for travel between downtown Lakewood and the Tillicum neighborhood without using l-5, for internal travel between the Lewis Main and McChord Field areas of JBLM, and for travel from Lewis Main to Lakewood without using l-5.

## P5: I-5 HOV and CD/Auxiliary Lanes Alternative - 2020 and 2040:

Alternative P5 would add an HOV lane in each direction and two sets of CD Lanes connected by auxiliary lanes. One set of CD lanes would link the ramps at the Mounts Road, Center Drive, and Steilacoom-

DuPont Road Interchanges. The other set would use an auxiliary lane to link ramps at the Berkeley Street and Thorne Lane Interchanges to Gravelly Lake Drive. These two sets of CD lanes would be connected with auxiliary lanes between the Steilacoom-DuPont CD lanes and the Berkeley CD lanes. For the 2020 analysis one of the existing GP lanes north of the Thorne Lane Interchange is assumed to be converted to an HOV lane. In the 2040 configuration, an HOV lane would be added to the existing four GP lanes at the north end and to the existing three lanes at the south end of the project.

P5a: I-5 HOV and CD/Auxiliary Lanes Alternative with Local Road Improvements - 2020 and 2040:
This alternative package would include all the improvements in the P5 - HOV and CD Lanes Alternative and would add the three local road improvement projects associated with Alternative Package P4a.

## P6: I-5 HOV and GP Lanes Alternative - 2020 and 2040:

Alternative P6 would add an HOV lane and a GP lane in each direction along I-5. A fourth GP lane would be added from Mounts Road to Thorne Lane in each direction. For the 2020 analysis, the HOV lanes would end south of the Steilacoom-DuPont Road Interchange and one of the existing GP lanes north of the Thorne Lane Interchange is assumed to be converted to an HOV lane. In the 2040 configuration, an HOV lane would be added to the existing four GP lanes at the north end of the project, and to the existing three lanes at the south end. For modelling purposes in 2040, the HOV lane is assumed to extend from Thurston County to Tacoma.

P6a: I-5 HOV and GP Lanes Alternative with Local Road Improvements - 2020 and 2040:
This alternative package would include all the improvements in the P6-HOV and GP Lanes Alternative and would add the three local road improvements associated with Alternative Package P4a.

## P7: I-5 HOV Lane Alternative - 2020 and 2040:

Alternative P7 would add an HOV lane in each direction along I-5. For 2020, the extra lanes would begin and end at the Center Drive Interchange and the inside northbound lane would become an HOV lane at the Steilacoom-DuPont Road Interchange. For the 2020 analysis one of the existing GP lanes north of the Thorne Lane Interchange is assumed to be converted to an HOV lane. In the 2040 configuration, an HOV lane would be added to the existing four GP lanes at the north end and to the existing three lanes at the south end of the project. For 2040 modelling purposes, the l-5 configuration assumes the HOV lanes extend from Thurston County to Tacoma. An existing GP lane in each direction north of the Thorne Lane Interchange would be converted into an HOV lane.

## P7a: I-5 HOV Lane Alternative with Local Road Improvements and Transit Enhancements - 2020 and 2040:

This alternative package would include all the improvements in the P7 - HOV Lanes Alternative and would add the enhanced transit improvements included in Alternative P2. It would also add the three local road improvement projects associated with Alternative Package P4a.

## P7b: I-5 HOV Lane Alternative with Local Road Improvements - 2020 and 2040:

This alternative package is the same as Alternative P7a except the enhanced transit improvements would not be not included.

Figure 1: Selected Local Road Improvements in Alternative Package P3


## Appendix F

## Build Alternative Intersection Analysis Summary

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Intersection Analysis Summary - 2020 Revised Build


Intersection Analysis Summary - 2020 Revised Build

| No. | Intersection | Control Type | Approach Road | Movement | AM PEAK HOUR |  |  |  |  |  | PM PEAK HOUR |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  | Post- <br> Process <br> Volume (vph) | LOSDelay <br> (sec) <br> Approach |  | LOS | Delay  <br> (sec) 95th <br> Queue <br> $(\mathrm{ft})$ <br> Movement |  | Post- <br> Process <br> Volume (vph) | LOS $\underbrace{}_{\text {Approach }}$Delay <br> (sec) |  | LOS | Delay <br> (sec) | 95th <br> Queue <br> (ft) <br> nt |
| 8 | Steilacoom DuPont Road / Barksdale Avenue / Wilmington Drive | Signal |  | Overall | 2,555 | D | 46.9 |  |  |  | 2,580 | D | 37.4 |  |  |  |
|  |  |  | Wilmington Drive | EB-L | 20 | D | 38.7 | D | 43.4 | 33 | 40 | D | 53.0 | D | 55.0 | 68 |
|  |  |  | Wilmington Drive | EB-T | 70 |  |  | D | 37.6 | 88 | 80 |  |  | D | 52.2 | 125 |
|  |  |  | Wilmington Drive | EB-R | 20 |  |  | D | 37.6 | 88 | 20 |  |  | D | 52.2 | 125 |
|  |  |  | Steilacoom-DuPont | WB-L | 245 | D | 42.7 | C | 30.7 | m116 | 330 | E | 59.1 | E | 62.2 | m275 |
|  |  |  | Steilacoom-DuPont | WB-T | 75 |  |  | C | 22.7 | m31 | 90 |  |  | D | 36.4 | m56 |
|  |  |  | Steilacoom-DuPont | WB-R | 890 |  |  | D | 47.7 | m78 | 485 |  |  | E | 61.1 | m64 |
|  |  |  | Steilacoom-DuPont | NB-L | 10 | C | 20.2 | D | 37.5 | 20 | 45 | B | 13.7 | D | 48.5 | 70 |
|  |  |  | Steilacoom-DuPont | NB-T | 75 |  |  | D | 41.0 | 82 | 135 |  |  | E | 56.5 | 170 |
|  |  |  | Steilacoom-DuPont | NB-R | 85 |  |  | A | 0.1 | 0 | 565 |  |  | A | 0.7 | 0 |
|  |  |  | Barksdale Avenue | SB-L | 985 | E | 56.7 | E | 57.0 | \#656 | 710 | C | 32.2 | C | 32.4 | 430 |
|  |  |  | Barksdale Avenue | SB-T | 65 |  |  | E | 56.4 | \#666 | 50 |  |  | C | 32.1 | 421 |
|  |  |  | Barksdale Avenue | SB-R | 15 |  |  | E | 56.4 | \#666 | 30 |  |  | C | 32.1 | 421 |
| 11 | I-5 NB Ramps / 41st Division Drive (Main Gate) | Cloverleaf <br> Merge / <br> Diverge |  | Overall |  | Cloverleaf merge/diverge Not Applicable for Synchro Analysis |  |  |  |  |  | Cloverleaf merge/diverge Not Applicable for Synchro Analysis |  |  |  |  |
|  |  |  | 1-5 Off Loop Ramp | EB-R |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  | I-5 Off-Ramp | WB-R |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  | 41st Division Drive | NB-T |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  | 41st Division Drive | NB-R |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  | SB-L |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  | 41st Division Drive | SB-T |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  | 41st Division Drive | SB-R |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  | Overall |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  | 1-5 Off Loop Ramp | EB-R |  |  |  |  |  |  |  |  |  |  |  |  |
|  | I-5 SB Ramps / | Cloverleaf | l-5 Off-ramp | WB-R |  |  |  |  |  |  |  |  |  |  |  |  |
| 12 | 41st Division Drive | Merge / | 41st Division Drive | NB-T |  |  | icabl | $\begin{gathered} \text { erg } \\ \text { Sy } \end{gathered}$ |  |  |  |  | icabl | or Syr | ro An | lysis |
|  |  |  | 41st Division Drive | NB-R |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  | 41st Division Drive | SB-T |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  | 41st Division Drive | SB-R |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  | Overall | 2,665 | A | 4.4 |  |  |  | 3,275 | A | 5.2 |  |  |  |
|  |  |  | 1-5 Off-ramp | EB-L | 170 |  |  | A | 7.5 | 24 | 225 |  |  | A | 6.4 | 26 |
|  |  |  | 1-5 Off-ramp | EB-T |  | A | 1.7 |  |  |  | 0 | A | 2.3 | A | 6.4 | 26 |
|  |  |  | 1-5 Off-ramp | EB-R | 630 |  |  | A | 0.1 |  | 400 |  |  | A | 0.0 |  |
| 13 | I-5 NB Ramps / | RAB | Berkeley Ave | NB-L |  |  |  |  |  |  |  |  |  |  |  |  |
| 13 | Berkelely Avenue | RAB | Berkeley Ave | NB-T | 240 | A | 2.7 | A | 5.4 | 27 | 880 | A | 6.2 | B | 10.8 | 146 |
|  |  |  | Berkeley Ave | NB-R | 445 |  |  | A | 1.3 | 19 | 1,305 |  |  | A | 3.1 | 146 |
|  |  |  | Berkeley Ave | SB-L | 60 |  |  | A | 7.4 |  | 5 |  |  | A | 4.3 |  |
|  |  |  | Berkeley Ave | SB-T | 1,120 | A | 7.0 | A | 7.2 |  | 460 | A | 4.2 | A | 4.2 |  |
|  |  |  | Berkeley Ave | SB-R |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  | Overall | 1,830 | B | 13.2 |  |  |  | 1,775 | A | 9.1 |  |  |  |
|  |  |  | 1 -5 Off-ramp | WB-L | 1,020 |  |  | B | 15.3 | 144 | 380 |  |  | A | 8.7 | 30 |
|  |  |  | 1 -5 Off-ramp | WB-T |  | B | 15.2 |  |  |  | 5 | A | 8.7 | A | 8.1 | 30 |
|  |  |  | 1-5 Off-ramp | WB-R | 185 |  |  | B | 14.9 | 144 | 5 |  |  | A | 8.1 | 30 |
| 14 | I-5 SB Ramps / | RAB | Berkeley Ave | NB-L | 140 |  |  | A | 4.2 |  | 545 |  |  | A | 7.1 |  |
|  | Berklely Avenue |  | Berkeley Ave | NB-T | 270 | A | 4.2 | A | 4.3 |  | 560 | A | 6.8 | A | 6.6 |  |
|  |  |  | Berkeley Ave | NB-R |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  | Berkeley Ave | SB-L |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  | Berkeley Ave | SB-T | 160 | B | 19.3 | B | 19.3 | 70 | 85 | B | 18.6 | B | 18.6 | 95 |
|  |  |  | Berkeley Ave | SB-R | 55 |  |  | B | 19.3 | 70 | 195 |  |  | B | 18.6 | 95 |
|  |  |  |  | Overall | 385 | C | 15.2 |  |  |  | 305 | A | 9.0 |  |  |  |
|  |  |  | Militia Dr | EB-L | 5 |  |  | C | 15.2 | 3 |  |  |  |  |  |  |
|  |  |  | Militia Dr | EB-T | 5 | C | 15.2 | C | 15.2 | 3 |  |  |  |  |  |  |
|  |  |  | Militia Dr | EB-R | 0 |  |  |  |  |  |  |  |  |  |  |  |
| 15 | Berkelely Avenue | two-way Stop | Union Ave | WB-L | 0 |  |  |  |  |  |  |  |  |  |  |  |
|  | / Union Avenue | Control | Union Ave | WB-T | 5 | A | 9.1 | A | 9.1 |  | 5 | A | 9.0 | A | 9.0 |  |
|  |  |  | Union Ave | WB-R | 150 |  |  | A | 9.1 | 15 | 115 |  |  | A | 9.0 | 11 |
|  |  |  | Berkeley Ave | SB-L | 205 |  |  | A | 7.2 | 14 | 175 |  |  | A | 7.2 | 12 |
|  |  |  | Berkeley Ave | SB-T |  | A | 7.2 |  |  |  |  | A | 7.2 |  |  |  |
|  |  |  | Berkeley Ave | SB-R | 15 |  |  | A | 7.2 | 14 | 10 |  |  | A | 7.2 | 12 |

Intersection Analysis Summary - 2020 Revised Build


Intersection Analysis Summary - 2020 Revised Build


Note: For Two-way Stop Control InterscetionS - Overall LOS and delay is based on worse approach/movement
Signalized and Non-signalized intersections analyzed with Synchro software
Rounadabout interscetion analyzed with Sidra software

Intersection Analysis Summary - 2040 Revised Build


Intersection Analysis Summary - 2040 Revised Build

| No. | Intersection | Control Type |  | Movement | AM PEAK HOUR |  |  |  |  |  | PM PEAK HOUR |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  | Post- <br> Process Volume (vph) | LOS App | Delay <br> (sec) <br> oach | LOS | Delay (sec) <br> Movem | 95th <br> Queue <br> (ft) <br> nt | Post- <br> Process Volume (vph) | LOS Ap | Delay <br> (sec) <br> oach | LOS | Delay <br> (sec) <br> Movem | 95th <br> Queue <br> (ft) <br> nt |
| 8 | Steilacoom - <br> DuPont Road/ Barksdale Avenue <br> / Wilmington Drive | Signal |  | Overall | 2,460 | D | 50.3 |  |  |  | 2,415 | C | 28.5 |  |  |  |
|  |  |  | Wilmington Drive | EB-L | 25 | E | 63.1 | E | 67.6 | 54 | 45 | D | 53.4 | D | 48.8 | 69 |
|  |  |  | Wilmington Drive | EB-T | 75 |  |  | E | 62.0 | 136 | 110 |  |  | D | 55.0 | 157 |
|  |  |  | Wilmington Drive | EB-R | 25 |  |  | E | 62.0 | 136 | 20 |  |  | D | 55.0 | 157 |
|  |  |  | Steilacoom-DuPont | WB-L | 245 | D | 53.9 | C | 33.7 | m137 | 180 | D | 47.3 | D | 43.1 | m125 |
|  |  |  | Steilacoom-DuPont | WB-T | 80 |  |  | C | 26.1 | m40 | 110 |  |  | D | 39.1 | m71 |
|  |  |  | Steilacoom-DuPont | WB-R | 1,125 |  |  | E | 60.3 | m214 | 530 |  |  | E | 50.5 | m43 |
|  |  |  | Steilacoom-DuPont | NB-L | 10 | C | 29.0 | E | 56.5 | 26 | 25 | B | 11.5 | E | 58.6 | 49 |
|  |  |  | Steilacoom-DuPont | NB-T | 90 |  |  | E | 62.9 | 135 | 135 |  |  | D | 48.2 | 172 |
|  |  |  | Steilacoom-DuPont | NB-R | 115 |  |  | A | 0.1 | 0 | 570 |  |  | A | 0.7 | 0 |
|  |  |  | Barksdale Avenue | SB-L | 585 | D | 47.0 | D | 47.0 | \#483 | 620 | B | 17.7 | C | 24.3 | 320 |
|  |  |  | Barksdale Avenue | SB-T | 70 |  |  | D | 47.0 | \#486 | 50 |  |  | B | 11.1 | 311 |
|  |  |  | Barksdale Avenue | SB-R | 15 |  |  | D | 47.0 | \#486 | 20 |  |  | B | 11.1 | 311 |
| 11 | I-5 NB Ramps / 41st Division Drive (Main Gate) | Merge / Diverge |  | Overall | 0 | Cloverleaf merge/diverge Not Applicable for Synchro Analysis |  |  |  |  |  | Cloverleaf merge/diverge Not Applicable for Synchro Analysis |  |  |  |  |
|  |  |  |  | EB-R |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  | WB-R |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  | NB-T |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  | NB-R |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  | SB-T |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  | SB-R |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 12 | I-5 SB Ramps / 41st Division Drive (Main Gate) | Merge / Diverge |  | Overall |  | Cloverleaf merge/diverge Not Applicable for Synchro Analysis |  |  |  |  |  | Cloverleaf merge/diverge Not Applicable for Synchro Analysis |  |  |  |  |
|  |  |  |  | EB-R |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  | WB-R |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  | NB-L |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  | NB-T |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  | NB-R |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  | SB-L |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  | SB-T |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  | SB-R |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 13 | I-5 NB Ramps / Berkelely Avenue | RAB |  | Overall | 2,865 | A | 4.5 |  |  |  | 2,520 | A | 4.6 |  |  |  |
|  |  |  | 1-5 Off-ramp | EB-L | 170 | A | 1.7 | A | 7.7 | 25 | 140 | A | 3.1 | A | 5.1 | 14 |
|  |  |  | 1-5 Off-ramp | EB-T |  |  |  |  |  |  | 0 |  |  | A | 5.1 | 14 |
|  |  |  | 1-5 Off-ramp | EB-R | 660 |  |  | A | 0.1 | 0 | 90 |  |  | A |  |  |
|  |  |  | Berkeley Ave | NB-T | 265 | A | 2.8 | A | 5.7 | 31 | 735 | A | 4.9 | A | 8.8 | 99 |
|  |  |  | Berkeley Ave | NB-R | 530 |  |  | A | 1.4 | 23 | 1,175 |  |  | A | 2.5 | 79 |
|  |  |  | Berkeley Ave | SB-T | 1,155 | A | 7.6 | A | 7.6 |  | 380 | A | 3.9 | A | 3.9 |  |
|  |  |  | Berkeley Ave | SB-R |  |  |  |  |  |  | 0 |  |  |  |  |  |
| 14 | I-5 SB Ramps / Berkelely Avenue | RAB |  | Overall | 1,995 | B | 16.7 |  |  |  | 1,475 | A | 8.7 |  |  |  |
|  |  |  | 1-5 Off-ramp | WB-L | 1,055 | B | 18.1 | B | 18.2 | 180 | 285 | A | 7.1 | A | 7.1 | 21 |
|  |  |  | 1 -5 off-ramp | WB-T |  |  |  |  |  |  | 5 |  |  | A | 6.7 | 21 |
|  |  |  | 1 -5 Off-ramp | WB-R | 235 |  |  | B | 17.7 | 180 | 0 |  |  | A | 6.7 | 21 |
|  |  |  | Berkeley Ave | NB-L | 140 | A | 4.4 | A | 4.2 |  | 535 | A | 6.1 | A | 6.4 |  |
|  |  |  | Berkeley Ave | NB-T | 295 |  |  | A | 4.4 |  | 340 |  |  | A | 5.6 |  |
|  |  |  | Berkeley Ave | NB-R |  |  |  |  |  |  | 0 |  |  |  |  |  |
|  |  |  | Berkeley Ave | SB-L |  | C | 29.6 |  |  |  | 0 | B | 17.6 |  |  |  |
|  |  |  | Berkeley Ave | SB-T | 185 |  |  | C | 29.6 | 112 | 95 |  |  | B | 17.6 | 99 |
|  |  |  | Berkeley Ave | SB-R | 85 |  |  | C | 29.6 | 112 | 215 |  |  | B | 17.6 | 99 |
| 15 | Berkelely Avenue / Union Avenue | Two-way Stop Control |  | Overall | 410 | C | 15.5 |  |  |  | 250 | B | 13.2 |  |  |  |
|  |  |  | Militia Dr | EB-L | 10 | C | 15.5 | C | 15.5 | 4 | 5 | B | 13.2 | B | 13.5 | 1 |
|  |  |  | Militia Dr | EB-T | 5 |  |  | C | 15.5 | 4 |  |  |  |  |  |  |
|  |  |  | Militia Dr | EB-R | 0 |  |  |  |  |  | 0 |  |  |  |  |  |
|  |  |  | Union Ave | WB-L |  | A | 9.3 |  |  |  |  | A | 8.9 |  |  |  |
|  |  |  | Union Ave | WB-T | 5 |  |  | A |  | 0 | 5 |  |  | A | 8.9 |  |
|  |  |  | Union Ave | WB-R | 180 |  |  | A | 9.3 | 19 | 60 |  |  | A | 8.9 | 5 |
|  |  |  | Berkeley Ave | SB-L | 195 | A | 7.2 | A | 7.2 | 13 | 175 | A | 7.4 | A | 7.4 | 12 |
|  |  |  | Berkeley Ave | SB-T |  |  |  | A | 7.2 | 13 |  |  |  |  |  |  |
|  |  |  | Berkeley Ave | SB-R | 15 |  |  |  |  |  | 5 |  |  | A | 7.4 | 12 |

Intersection Analysis Summary - 2040 Revised Build


Intersection Analysis Summary - 2040 Revised Build


Note: For Two-way Stop Control InterscetionS - Overall LOS and delay is based on worse approach/movement
Synchro Analysis for Signalized and non-signalized intersections
Sidra Analysis for roundabouts

## Appendix G

## Collision Summary of ISATe Model Results

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## Summary of ISATe model results per scenario

| Study Year | Data Source | Scenario | Mainline |  | Ramps |  | Terminals |  | Total <br> Crashes | Total Crashes Per MVM |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Crashes | Crashes Per MVM | Crashes | Crashes Per MVM | Crashes | Crashes Per MEV |  |  |
| 2014 | Existing Data | No Build | 330 | 0.88 | 52 | 2.16 | 10 | 0.11 | 392 | 1.09 |
| 2014 | Model outputs | No Build | 319 | 0.85 | 26 | 1.09 | 35 | 0.41 | 380 | 1.06 |
| 2020 | Model outputs | No Build | 364 | 0.89 | 27 | 1.13 | 40 | 0.39 | 431 | 1.11 |
| 2040 | Model outputs | No Build | 443 | 0.96 | 25 | 1.05 | 45 | 0.43 | 513 | 1.14 |
| 2020 | Model outputs | Build | 377 | 0.91 | 30 | 1.15 | 42 | 0.41 | 449 | 1.06 |
| 2040 | Model outputs | Build | 491 | 0.96 | 30 | 1.13 | 42 | 0.40 | 563 | 1.10 |

MVM = Million Vehicle Miles
MEV = Million Entering Vehicle


[^0]:    ${ }^{1}$ Point Defiance Bypass Project - Transportation Discipline Report, WSDOT, September, 2012

[^1]:    Notes: * Intersection operations analysis is based on direct output from the Meso Model which reflects impacts of traffic queuing through adjacent intersection.
    ** The I-5 NB Ramps / Center Drive intersection was redesigned in 2015. This new design is reflected in the 2020 and 2040 analysis.
    LOS E and LOS F values shown in bold.

[^2]:    N: \Projects $\backslash 0930$ H.W. Lochner Inc\0930.03 I-5 JBLM $\backslash$ Phase 13 - Task AD - Kickoff and MA Methods \& Assumptions $\backslash 2013-0507$ FINAL Methods and Assumptions.docxx

